

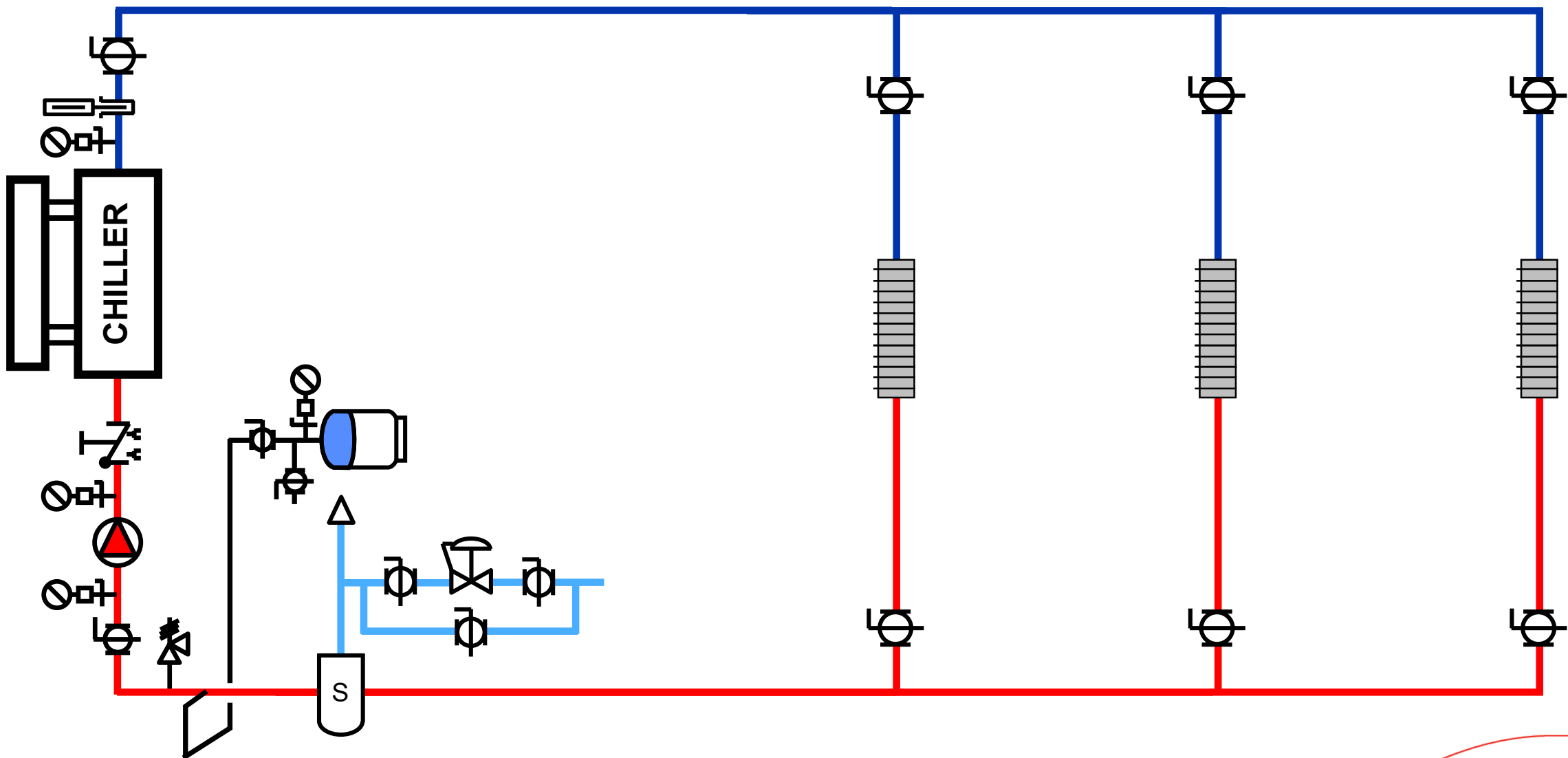
# Large Chilled Water System

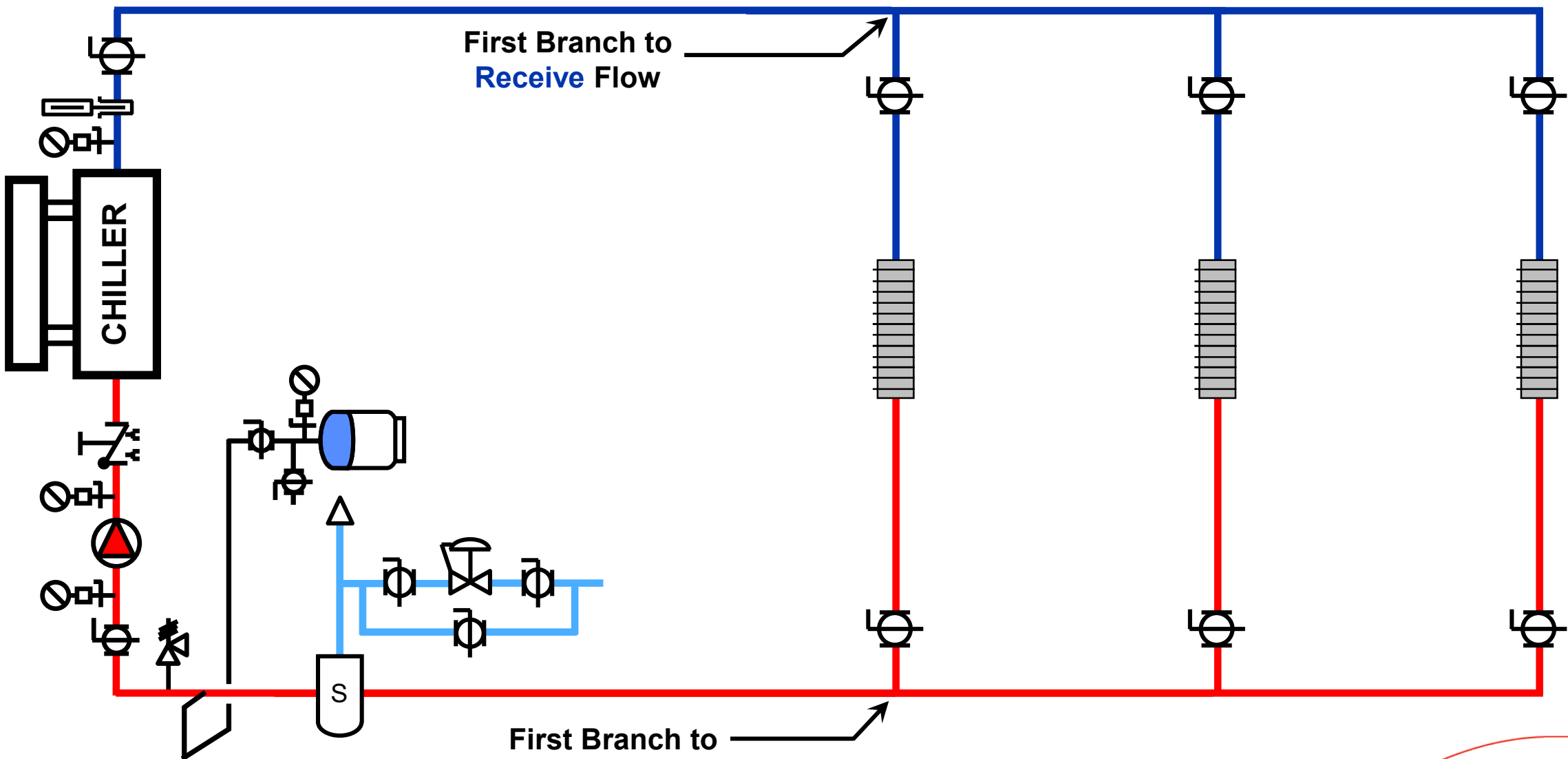
## Design Seminar

Courtesy of Oslin Nation Company

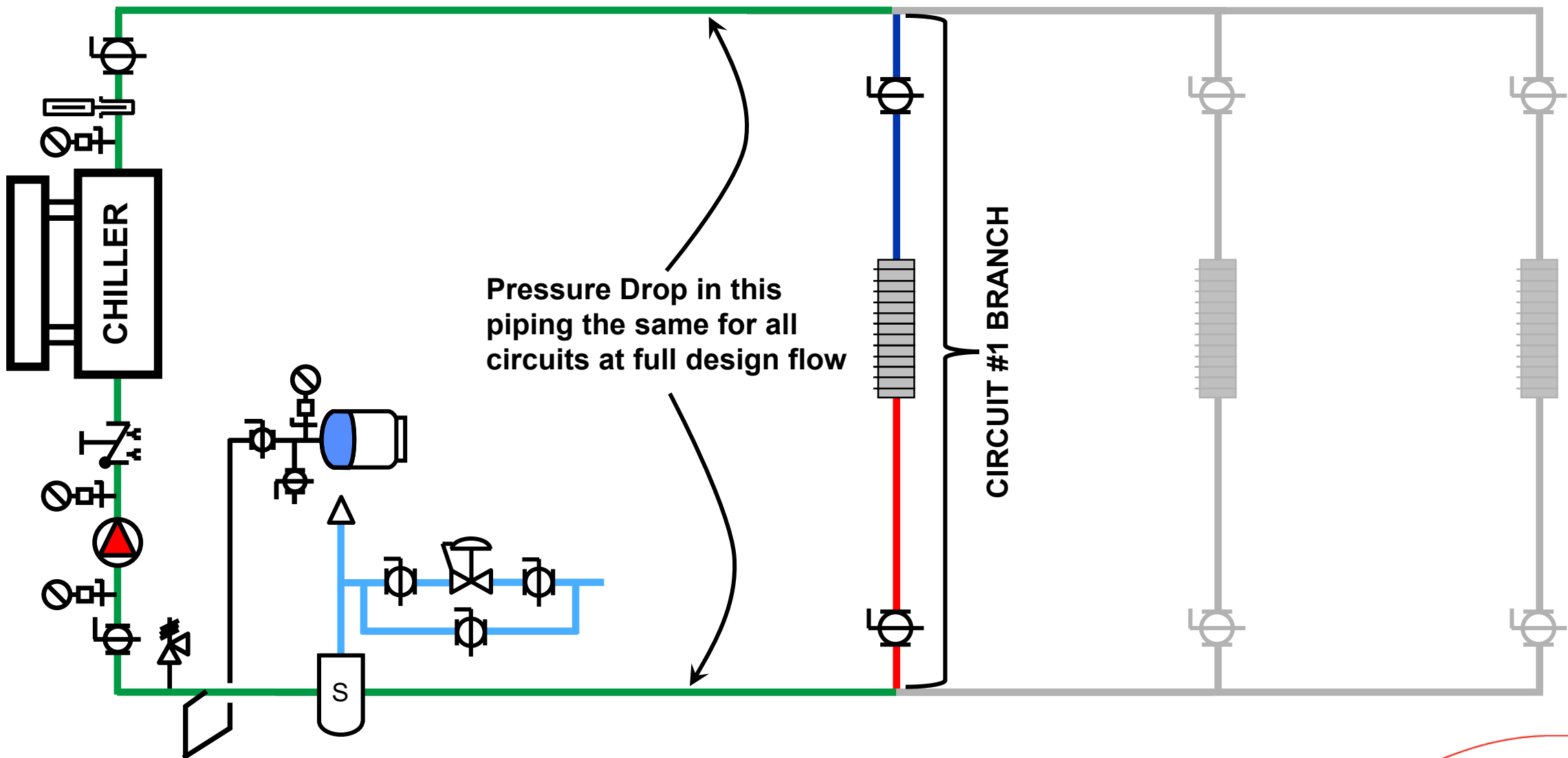
### Distribution Piping Strategies

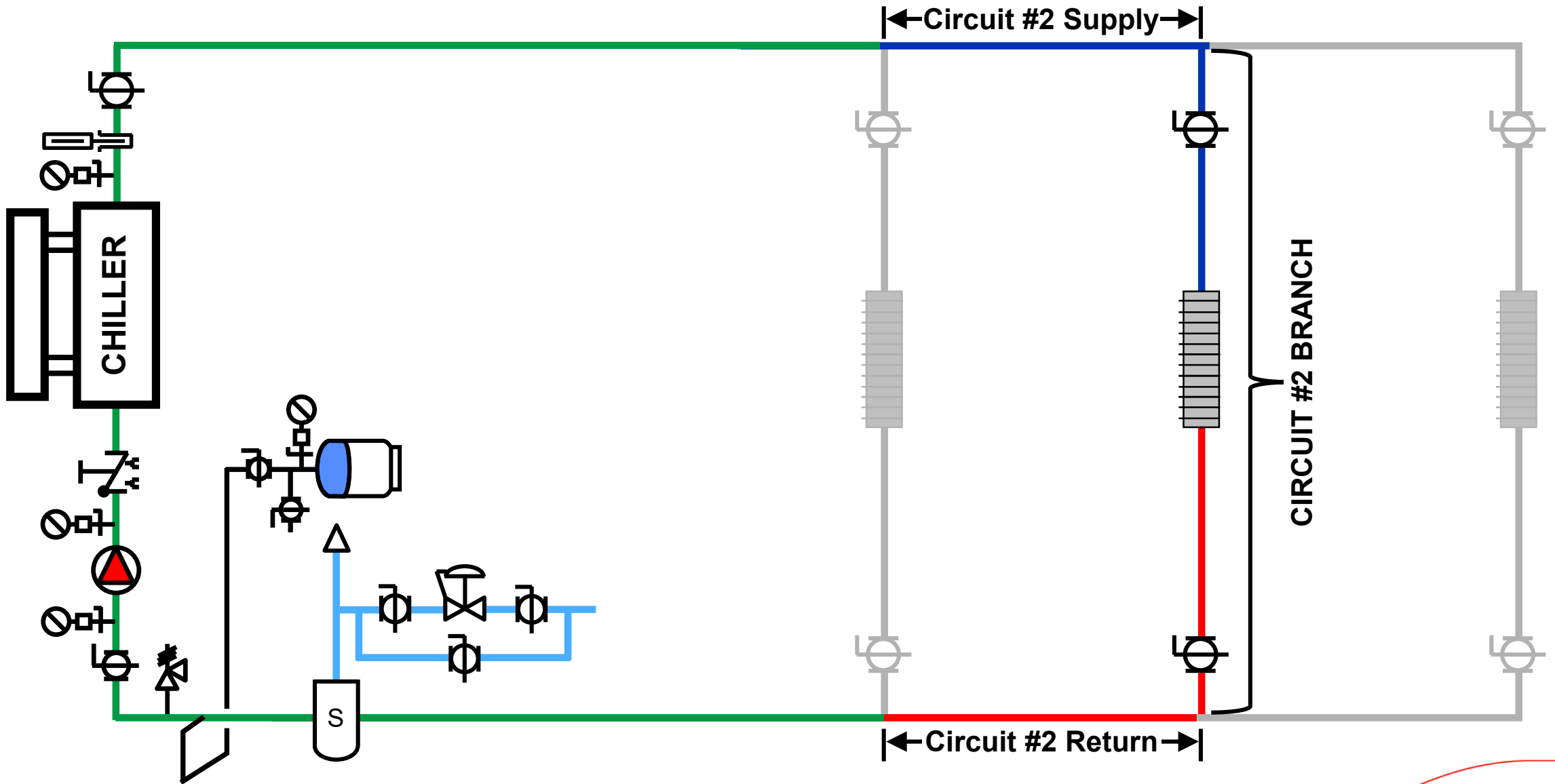
## 2-Pipe Parallel Circuits

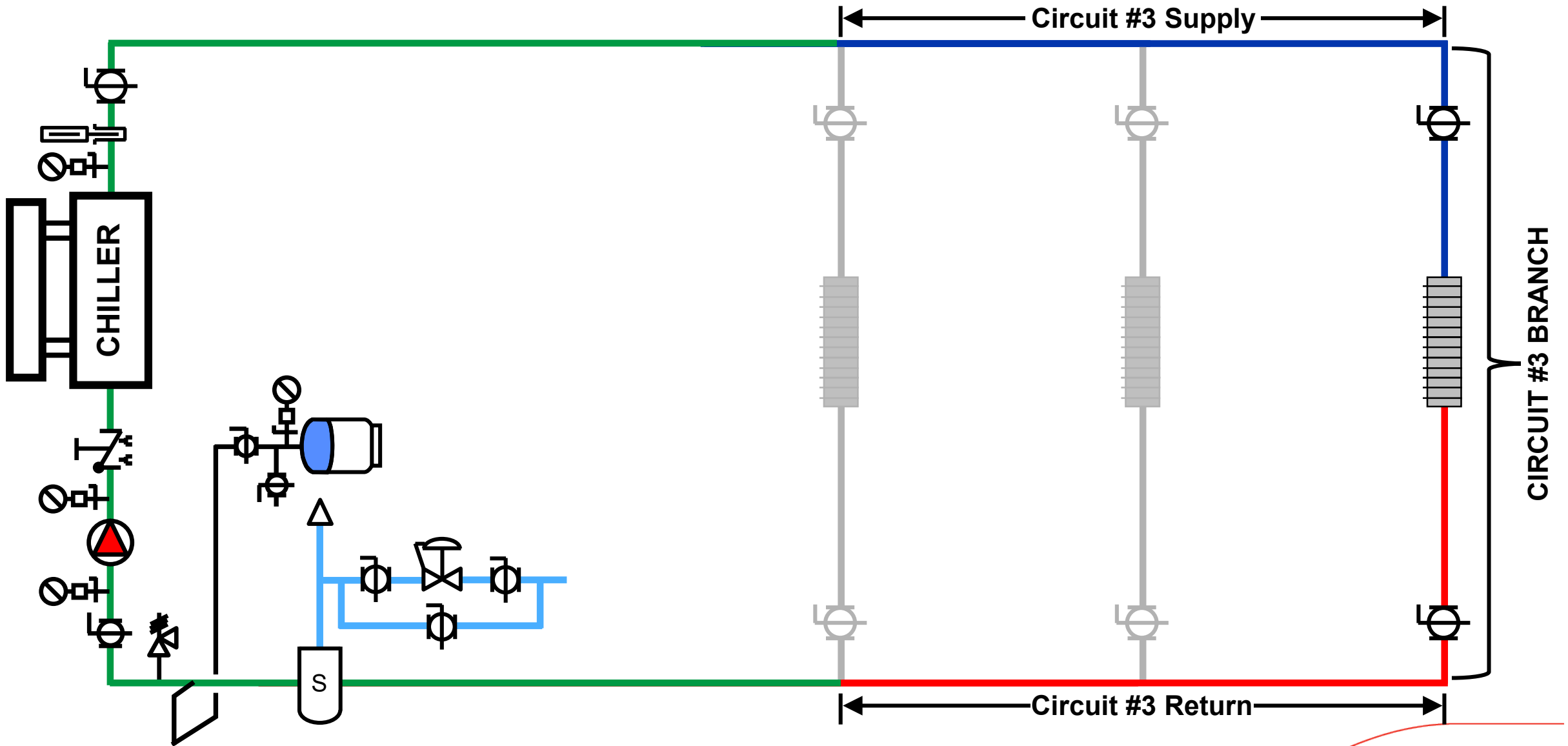




First Branch to  
Return Flow

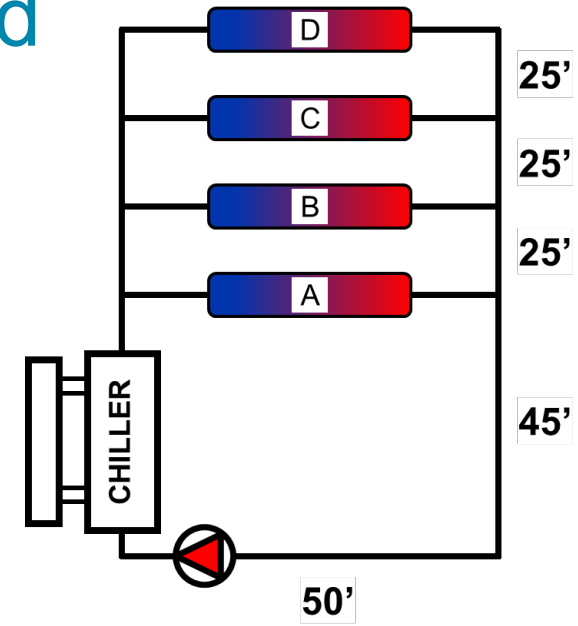
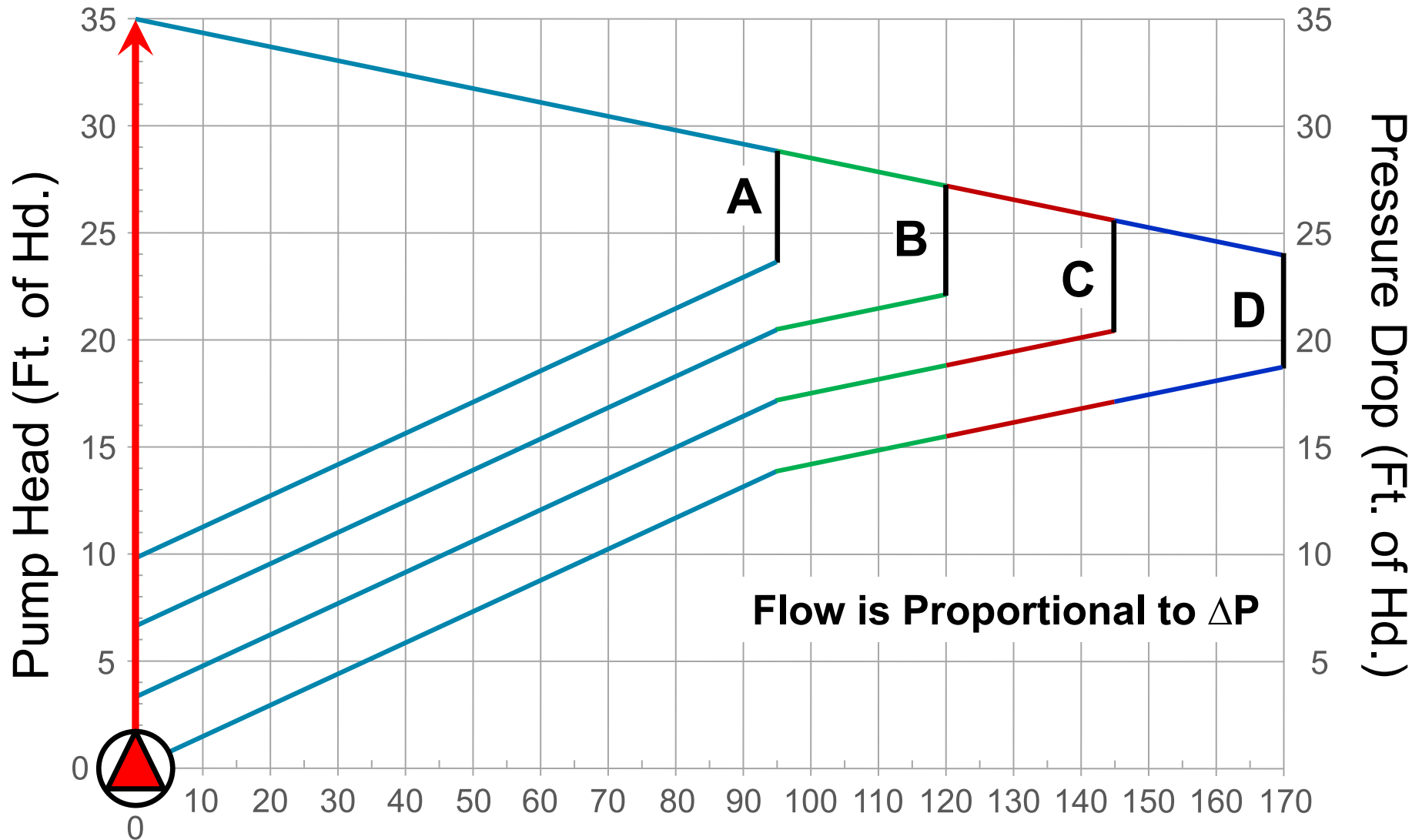






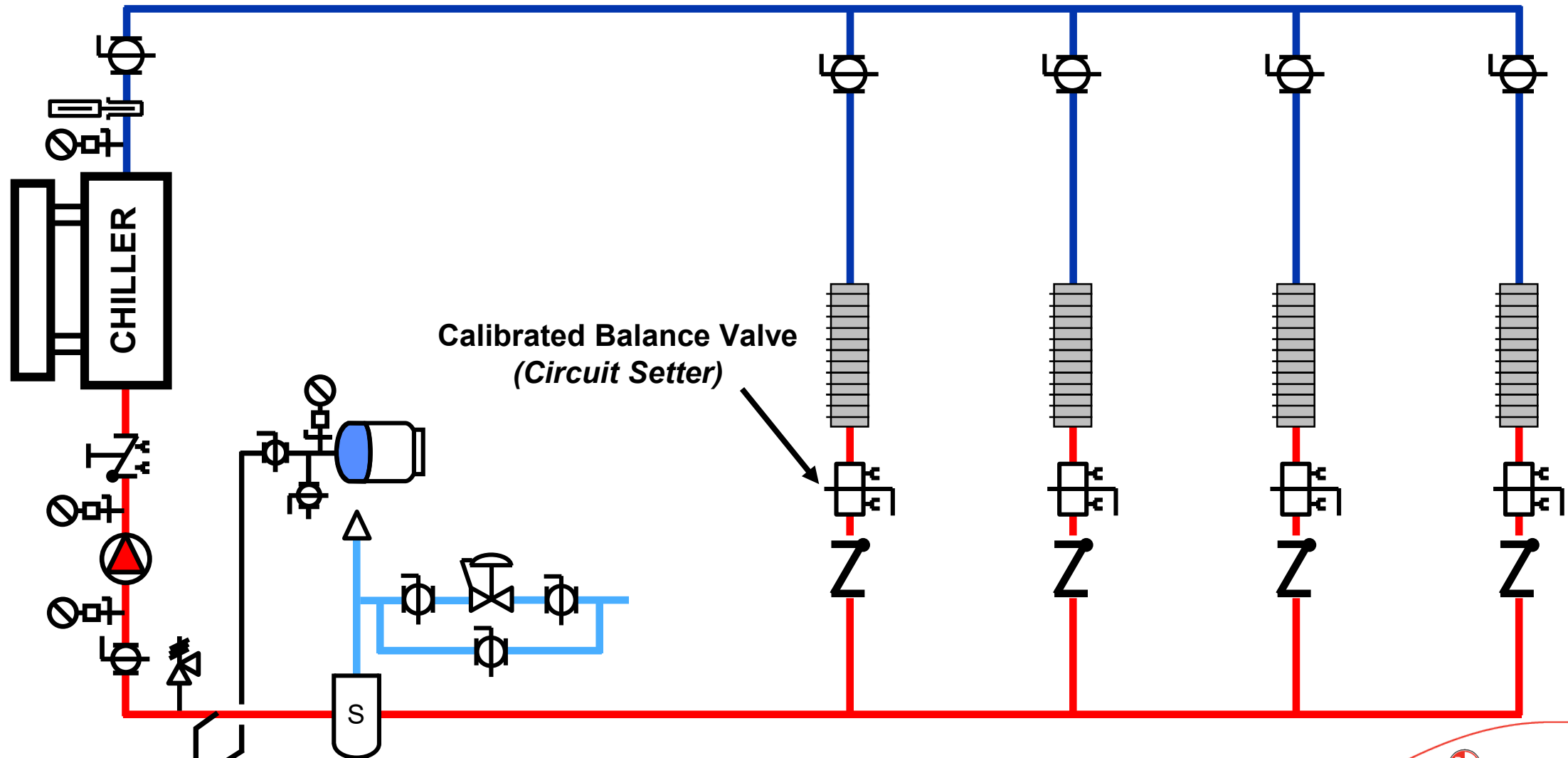
# System Pressure Gradient Diagram – Not Balanced

## 2-Pipe Direct Return





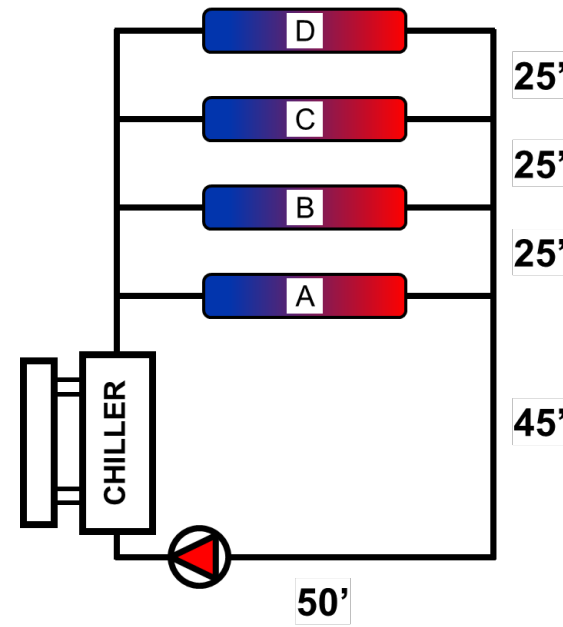
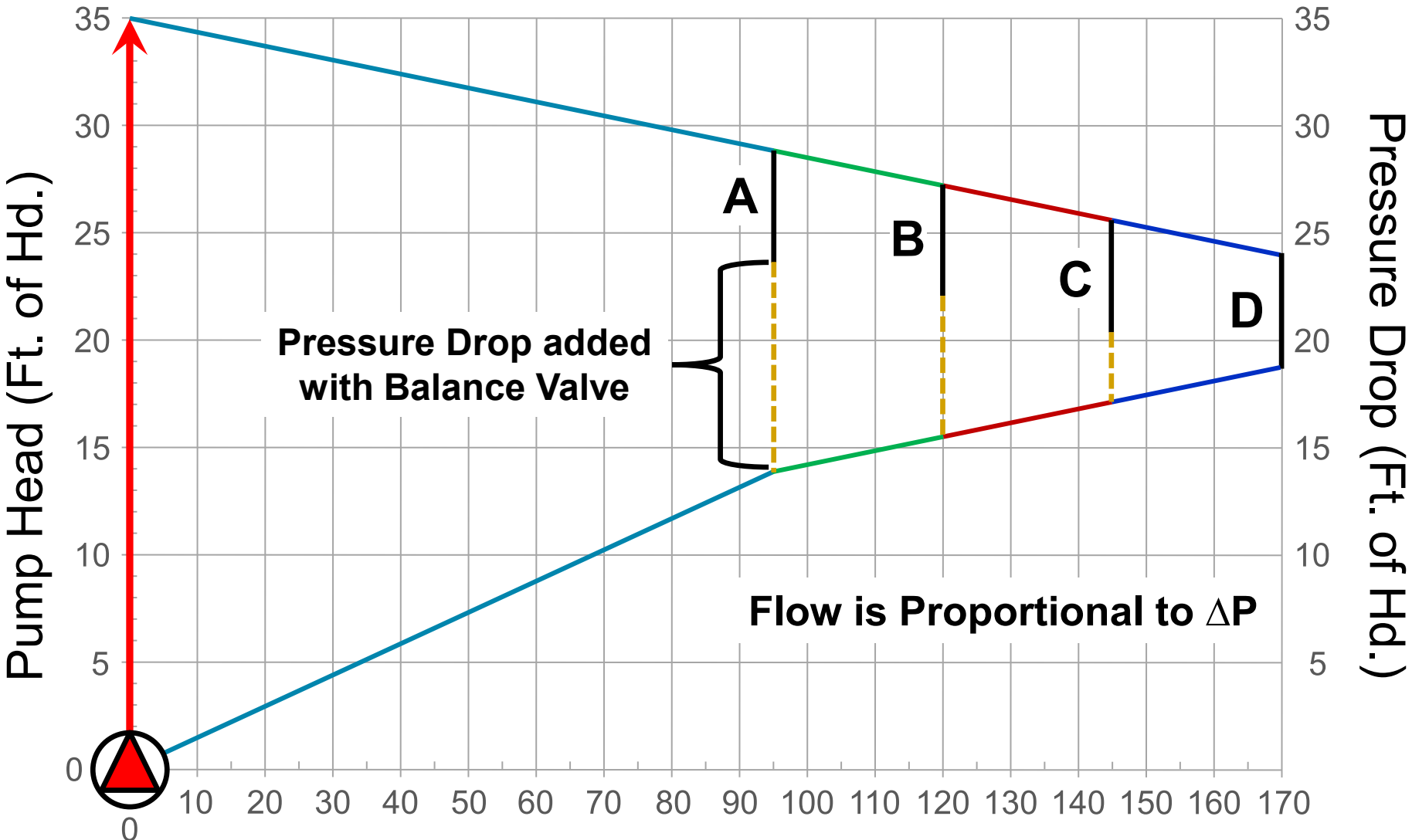
# 2-Pipe Parallel Circuits – Direct Return Flow Distribution



Calibrated Balance Valve  
(Circuit Setter)

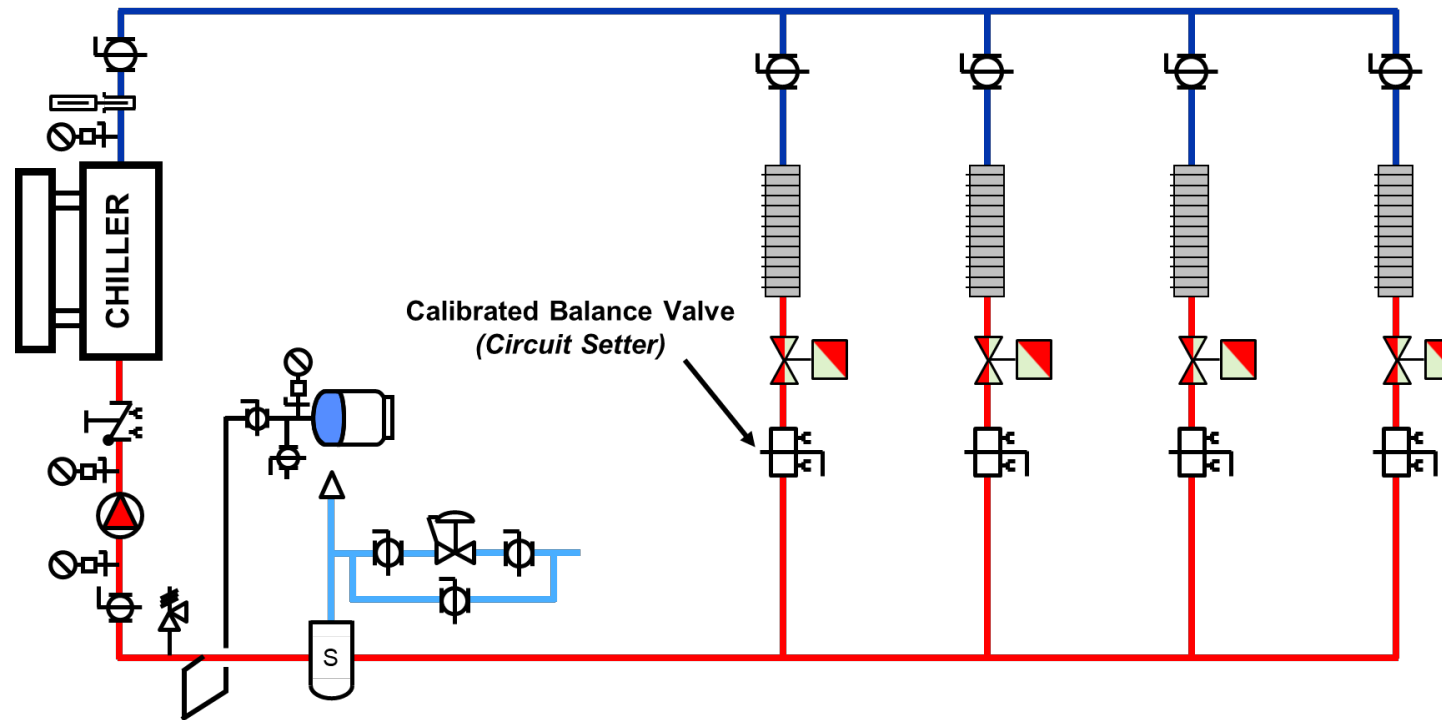
# System Pressure Gradient Diagram – Balanced

## 2-Pipe Direct Return



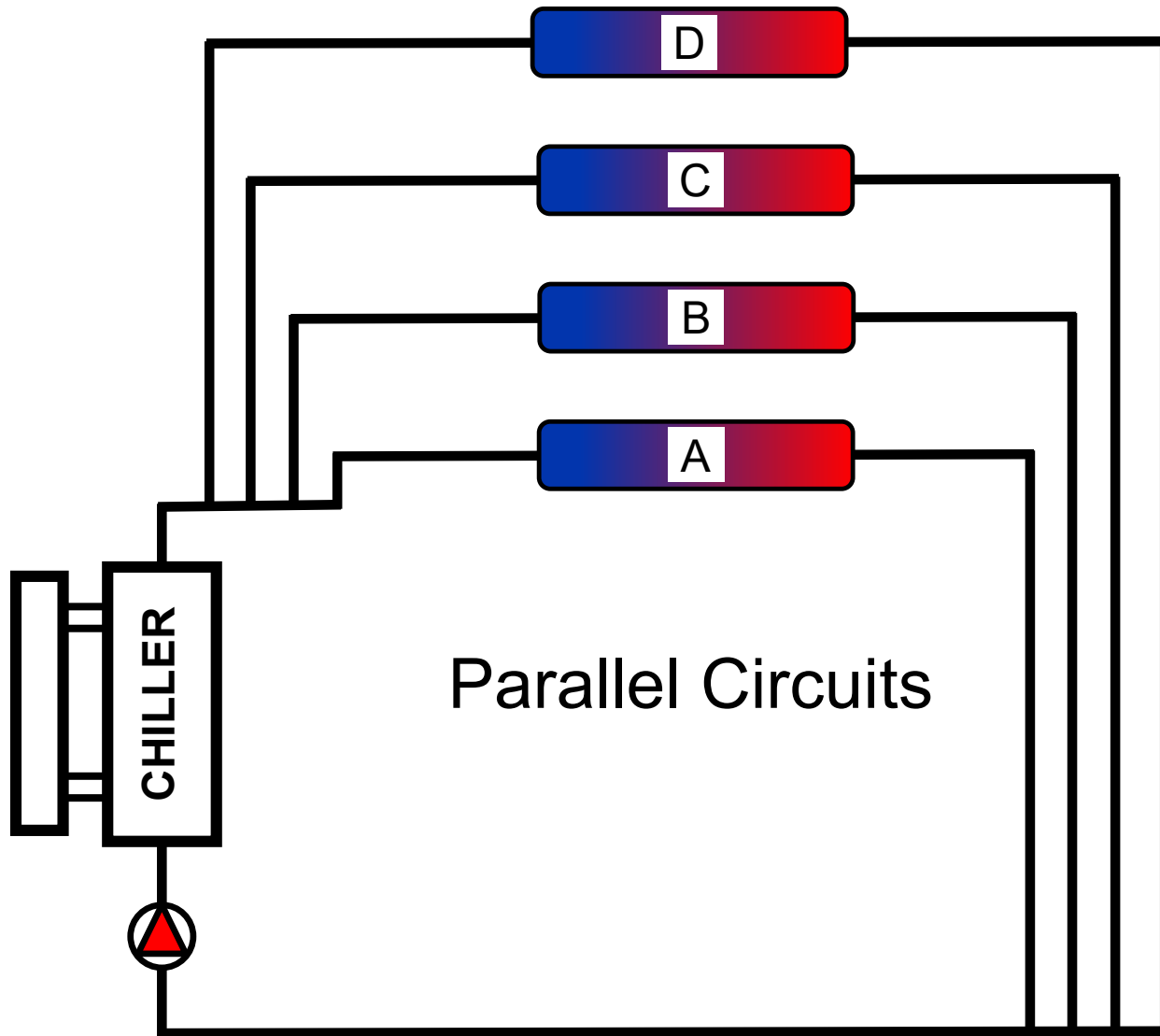
# REMINDER: System Head Loss for Closed Loop Pump Sizing

## Parallel Loops

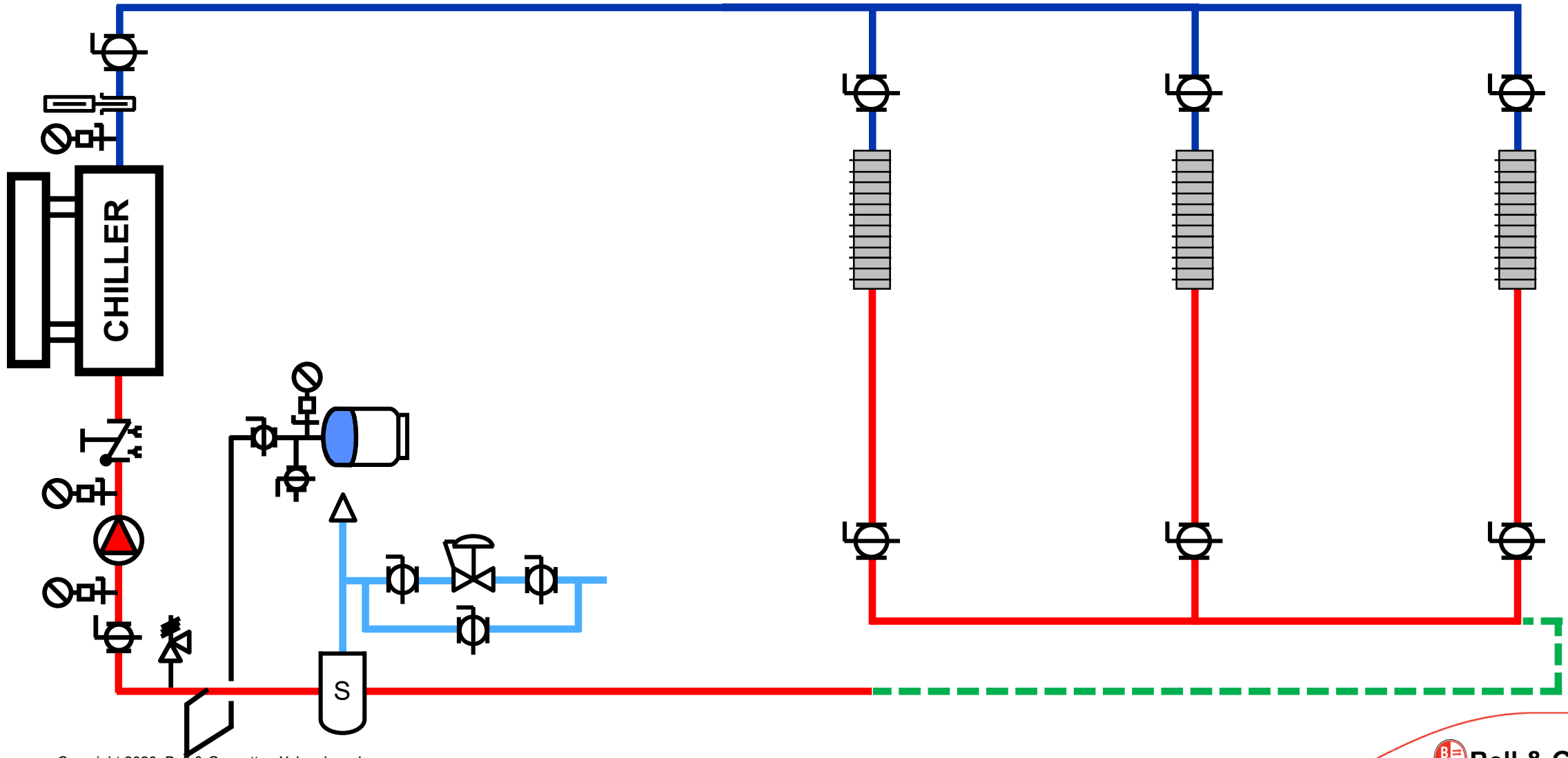


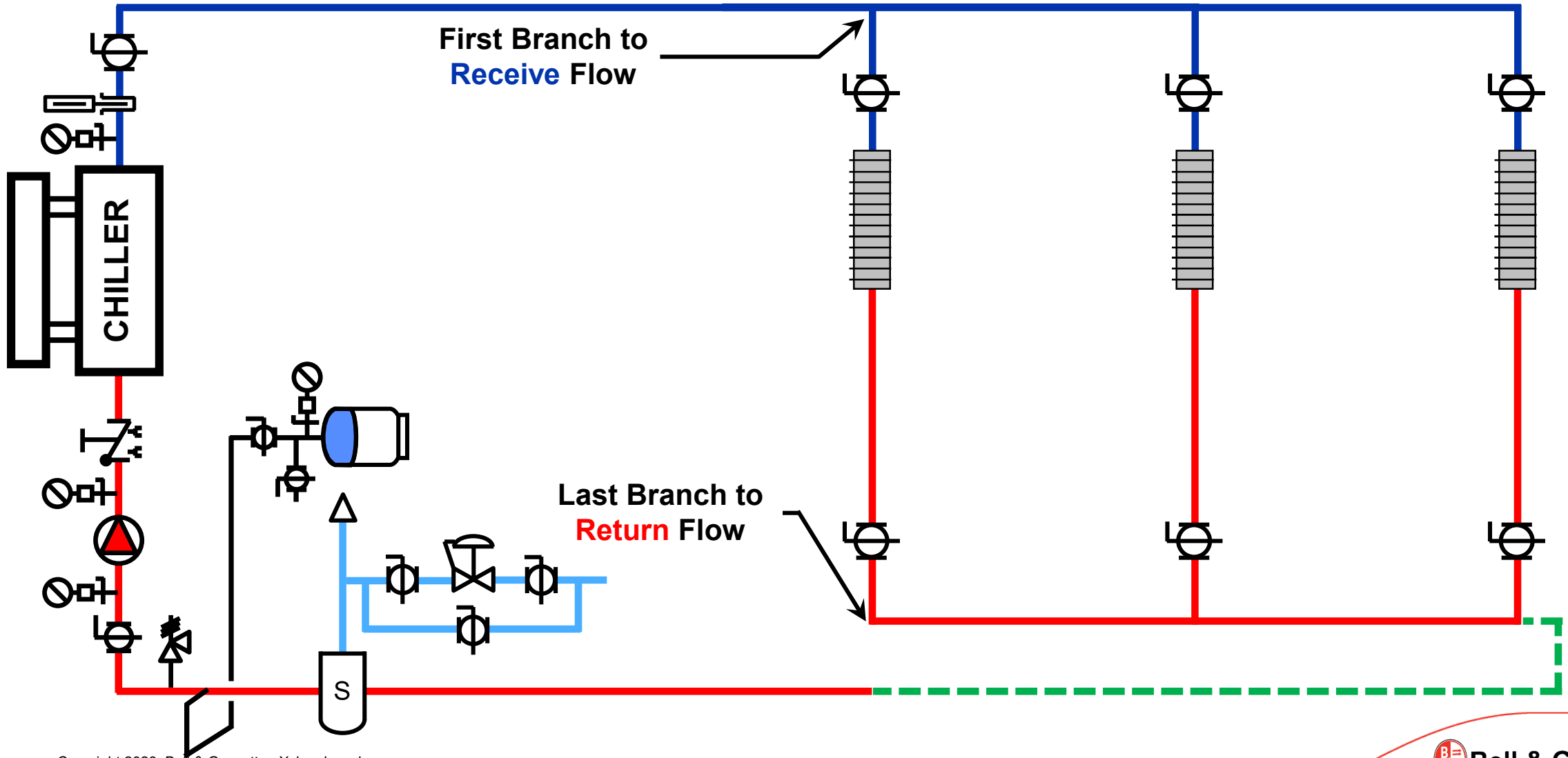
**Total System Head Loss = B+C for Critical Circuit**

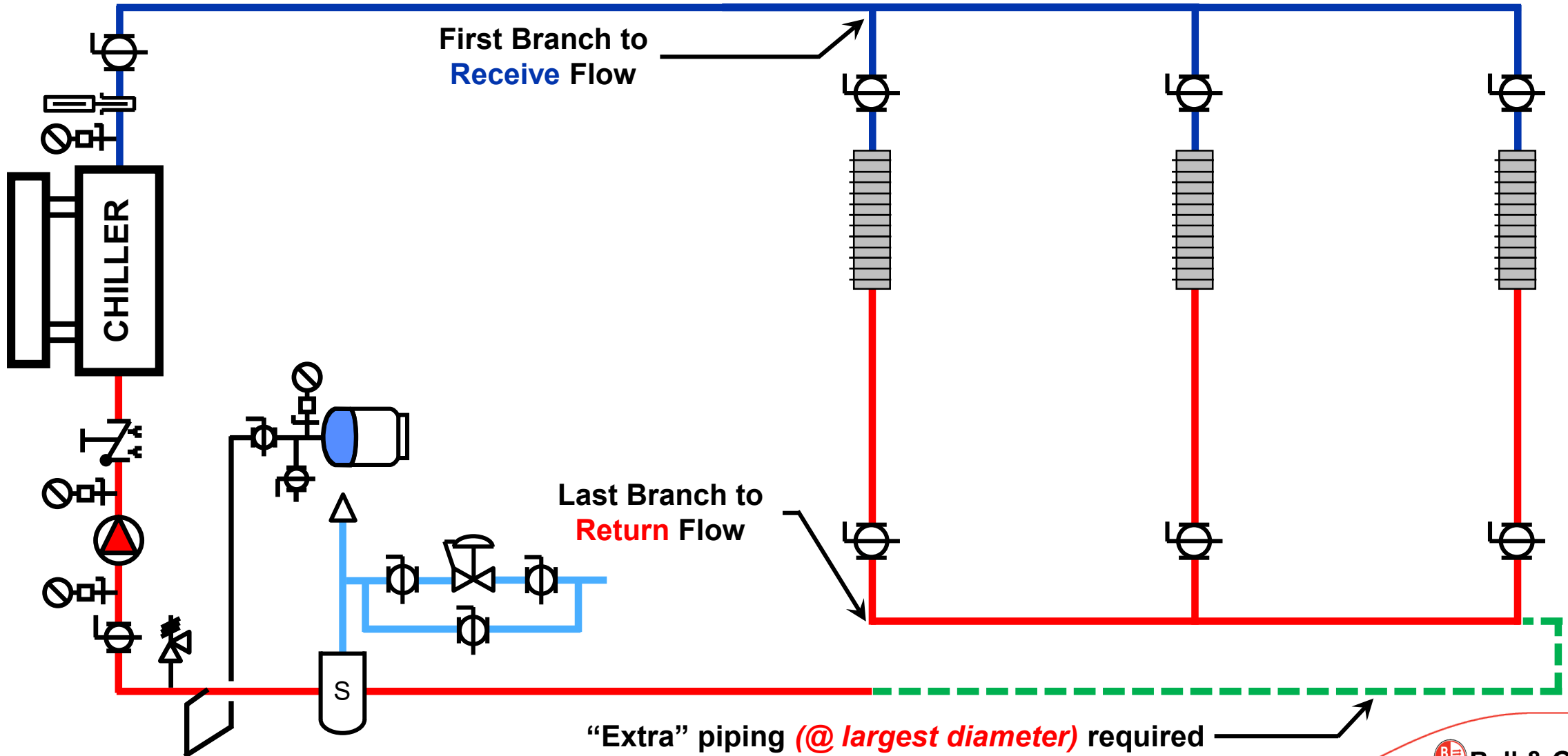
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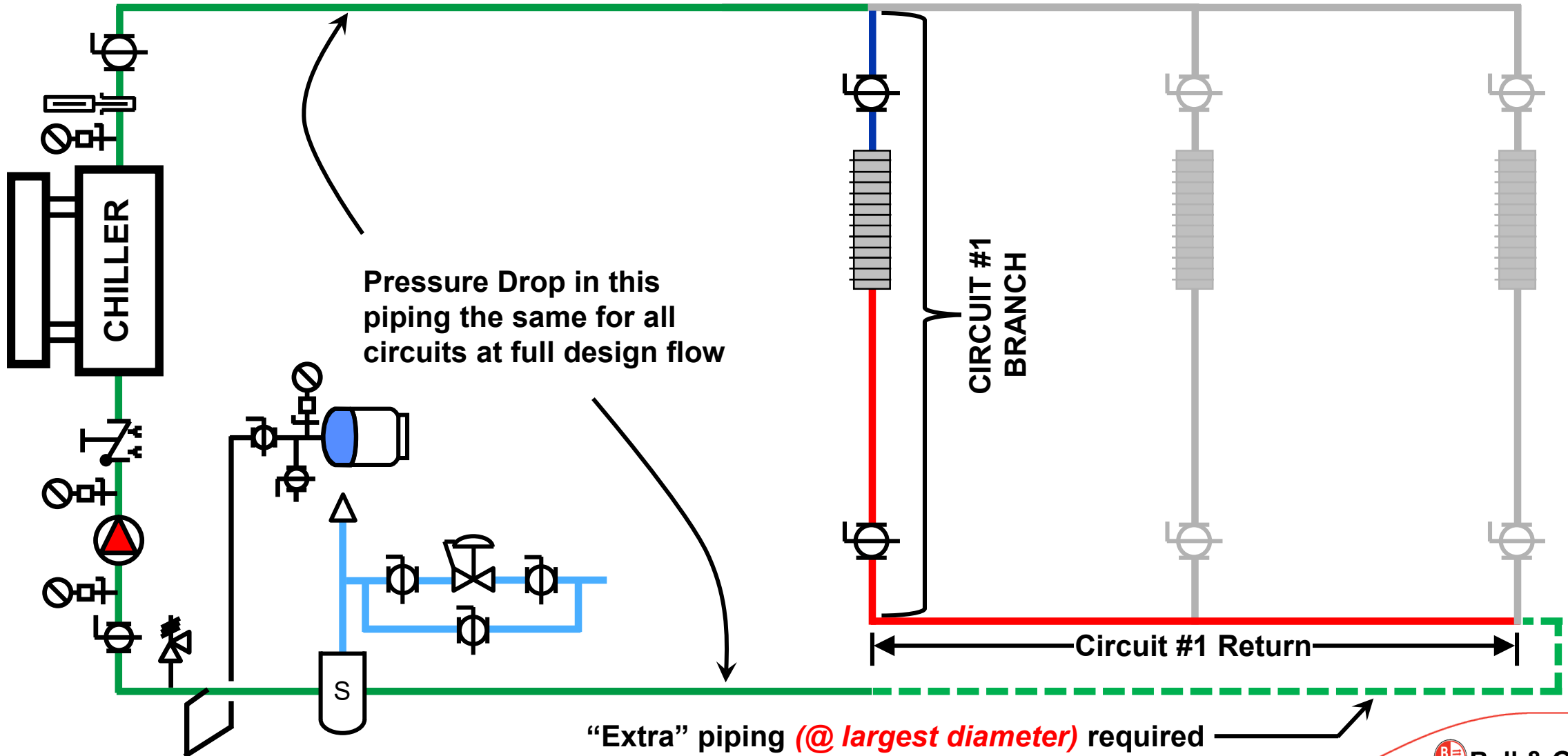
Parallel Circuits





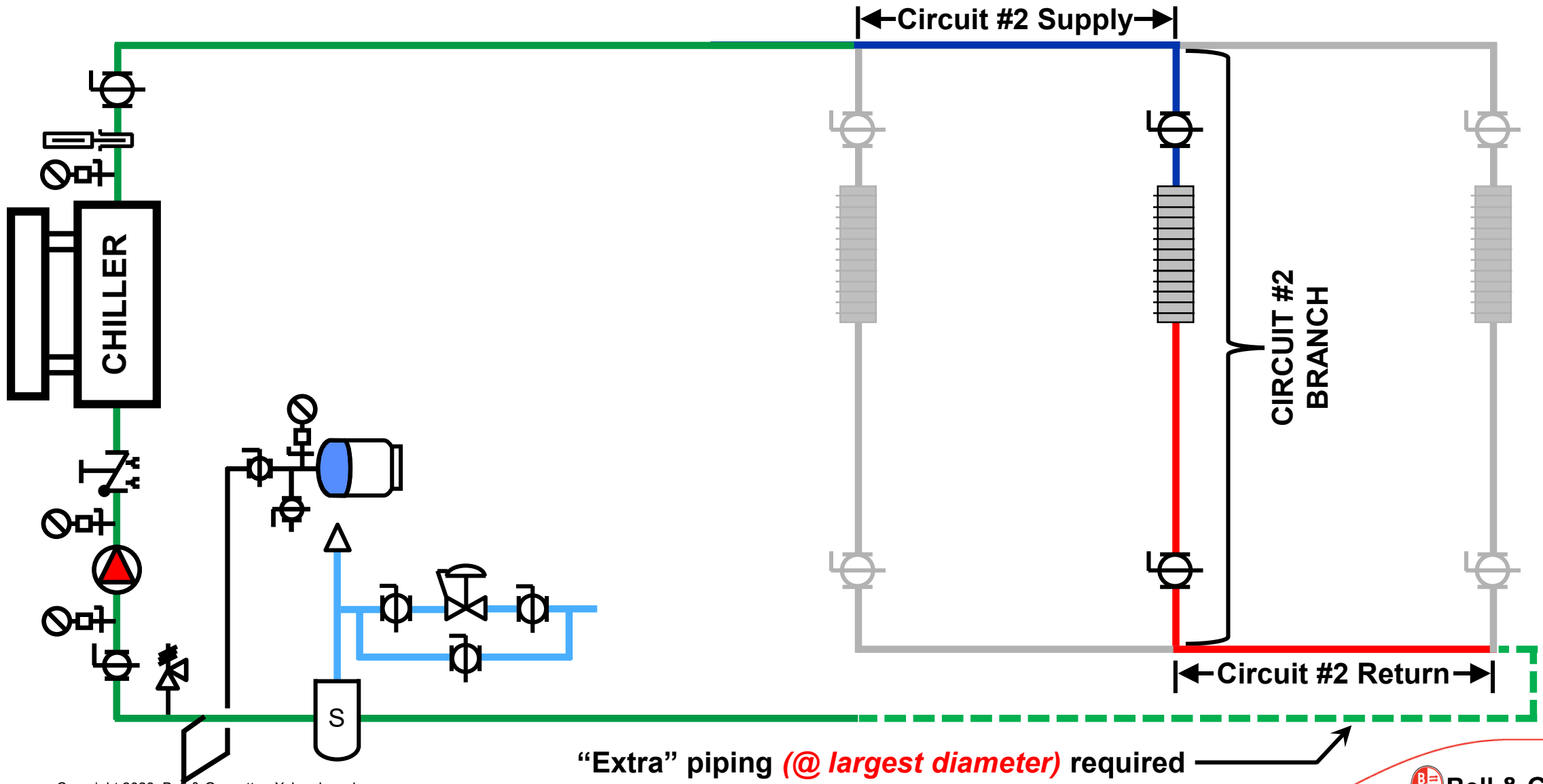


“Extra” piping (*@ largest diameter*) required to return all flow back to boiler.

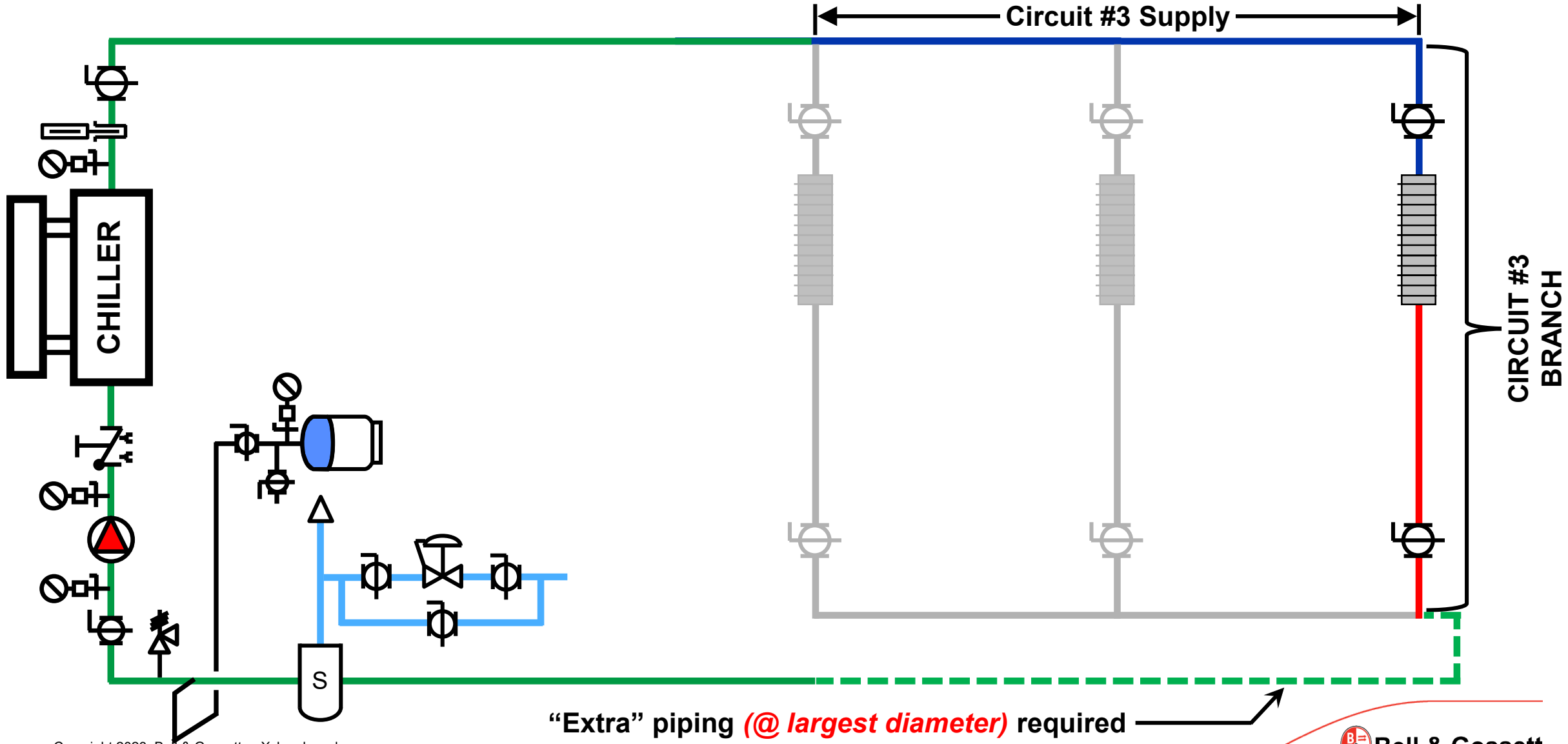


**“Extra” piping (@ largest diameter) required to return all flow back to boiler.**





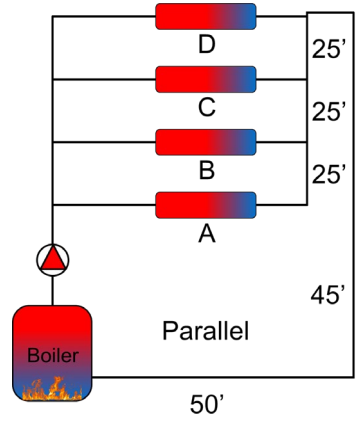
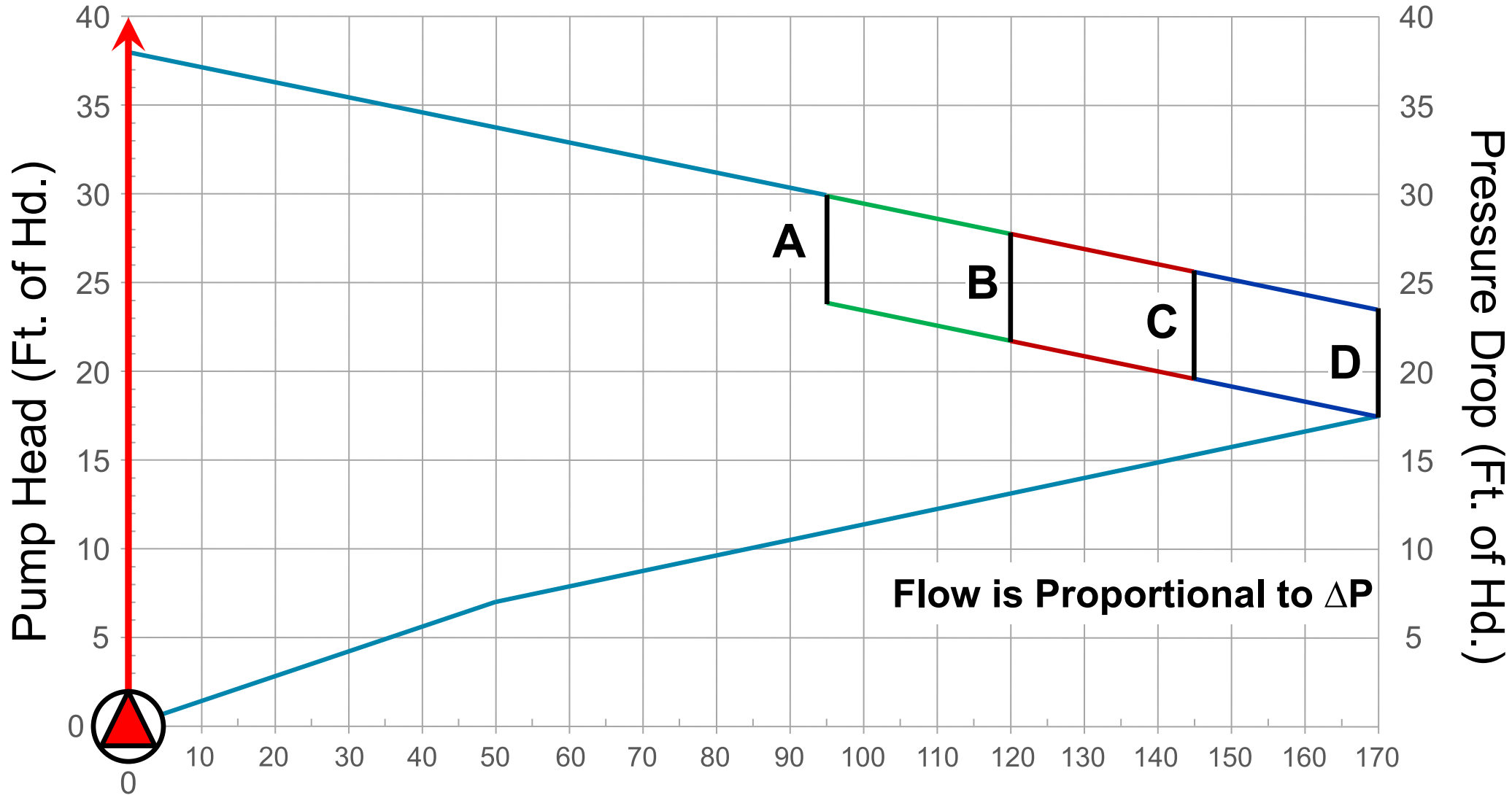
"Extra" piping (@ largest diameter) required to return all flow back to boiler.

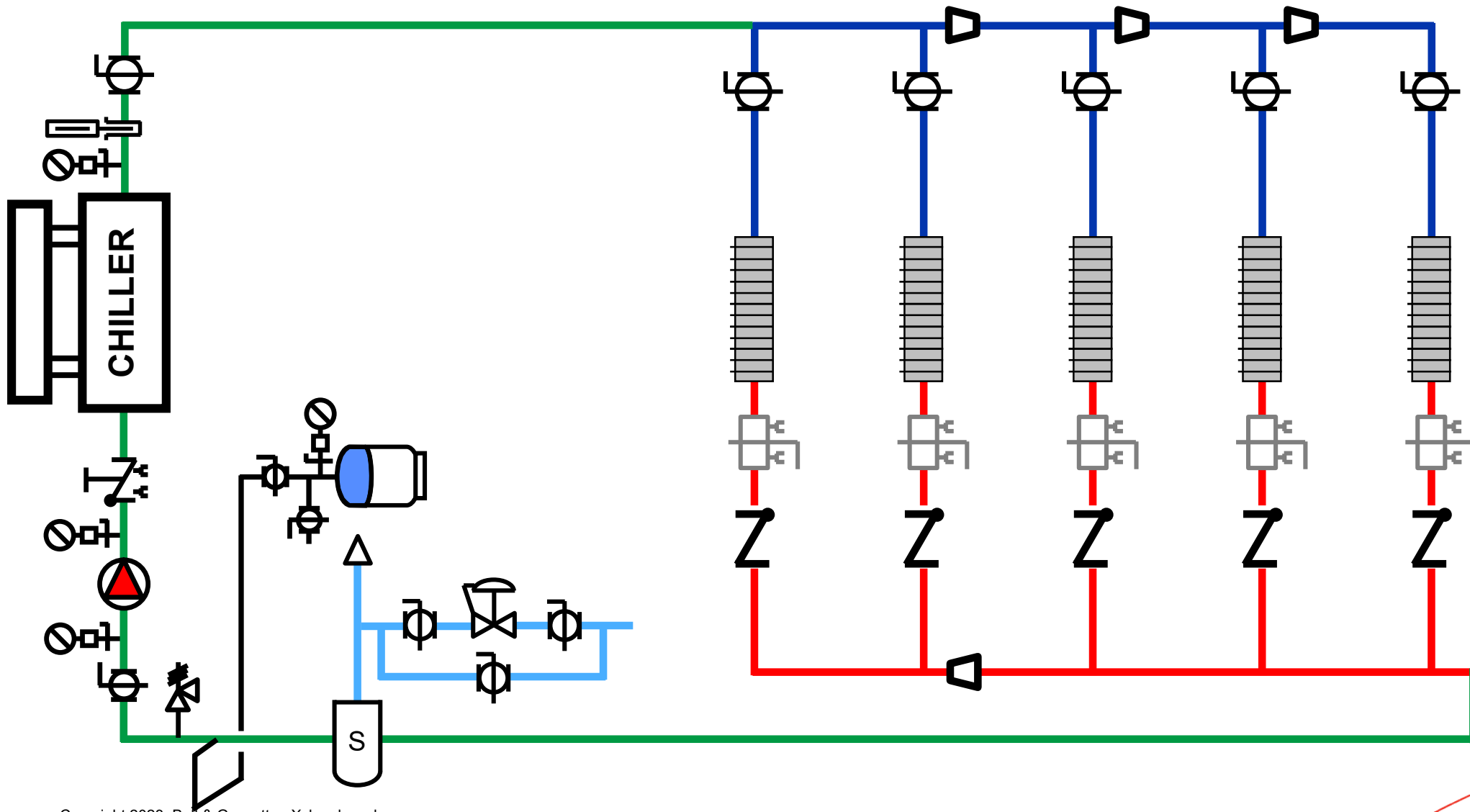


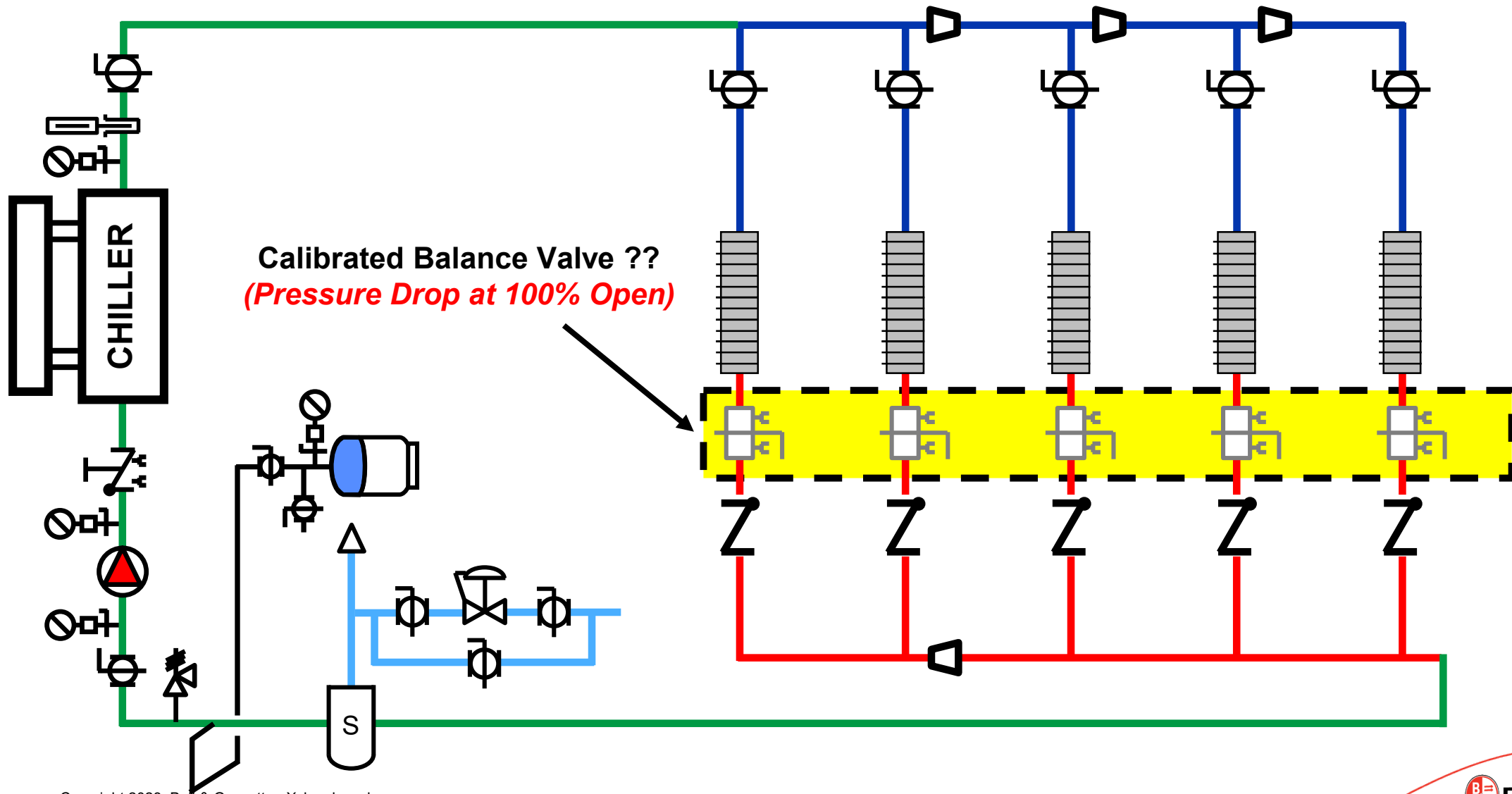
“Extra” piping (*@ largest diameter*) required to return all flow back to boiler.

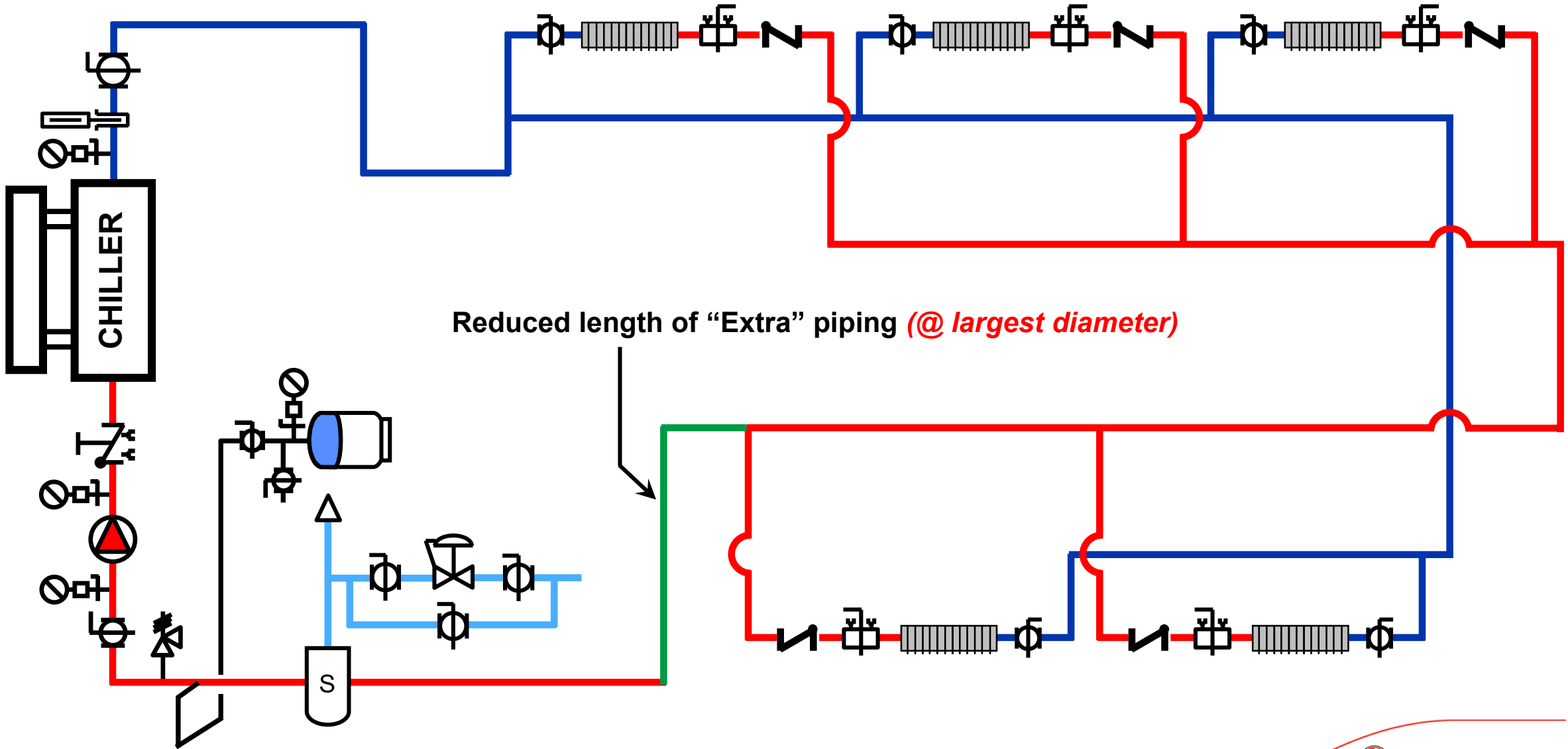
# System Pressure Gradient Diagram – Balanced??

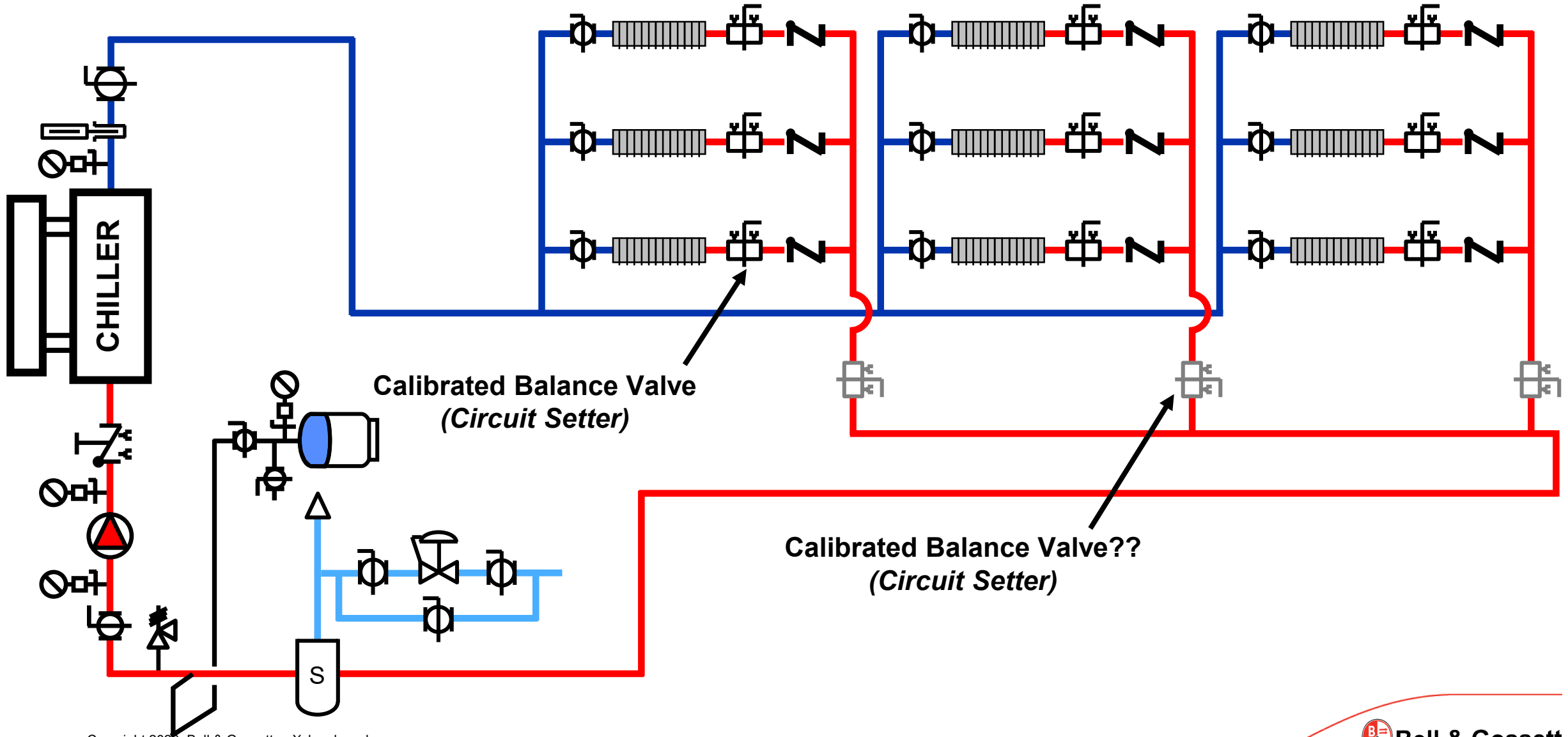
## 2-Pipe Reverse Return

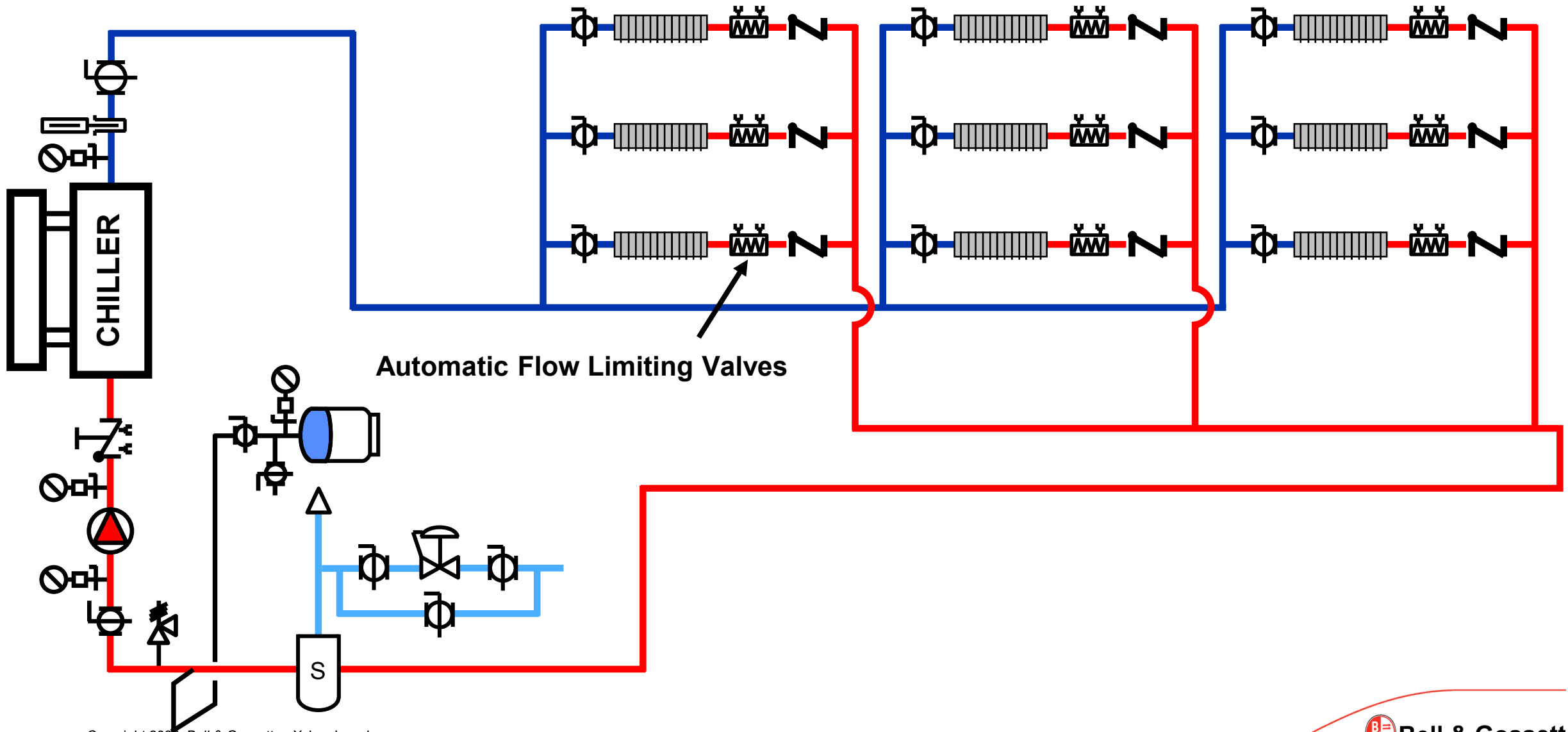






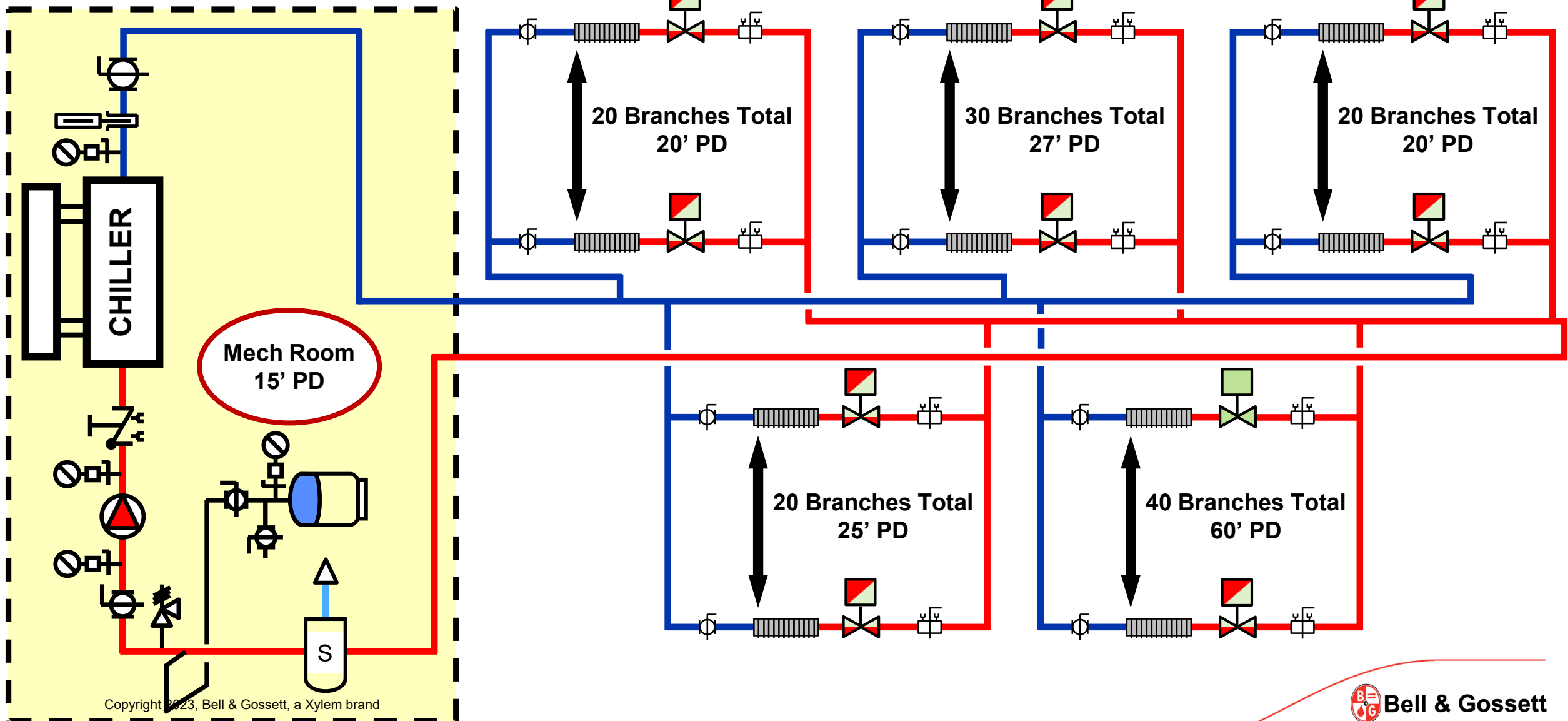


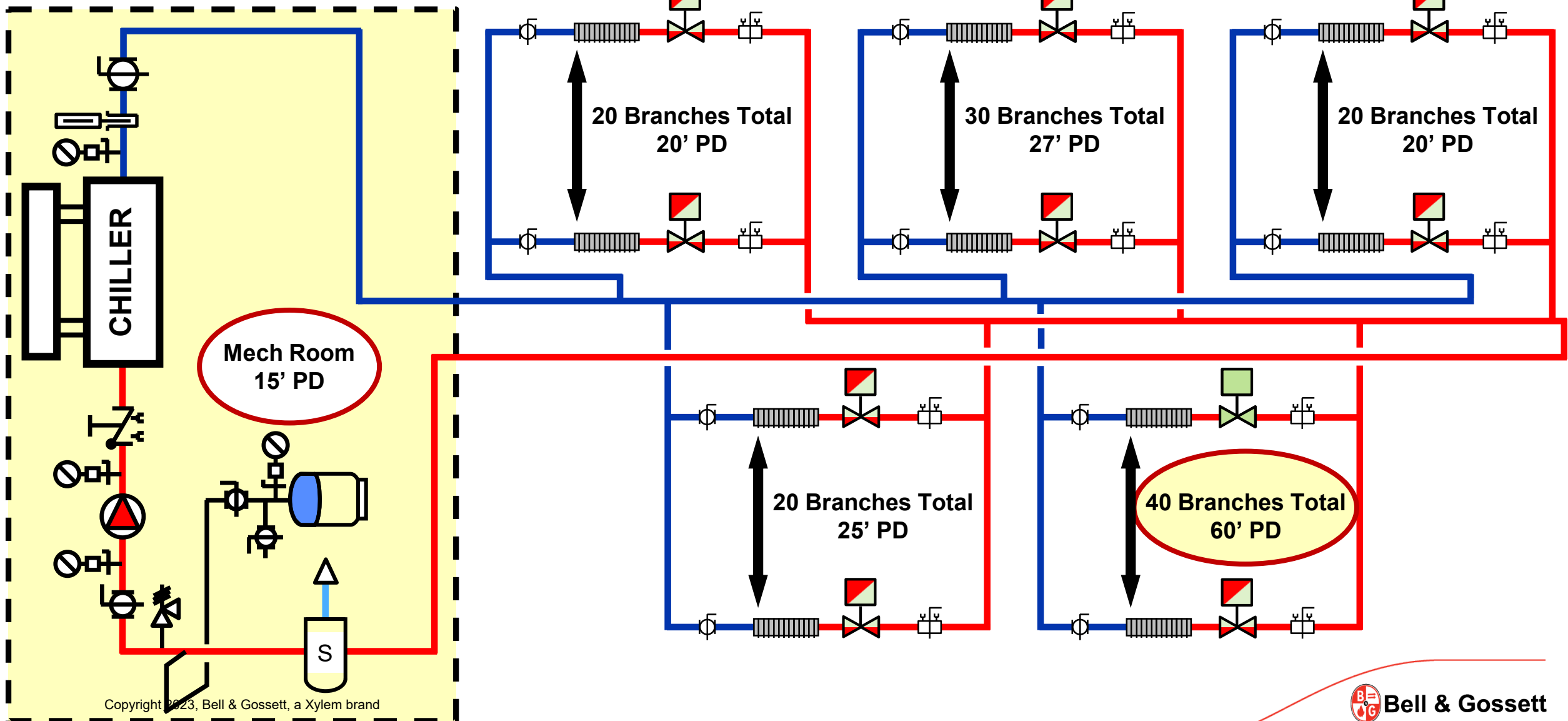




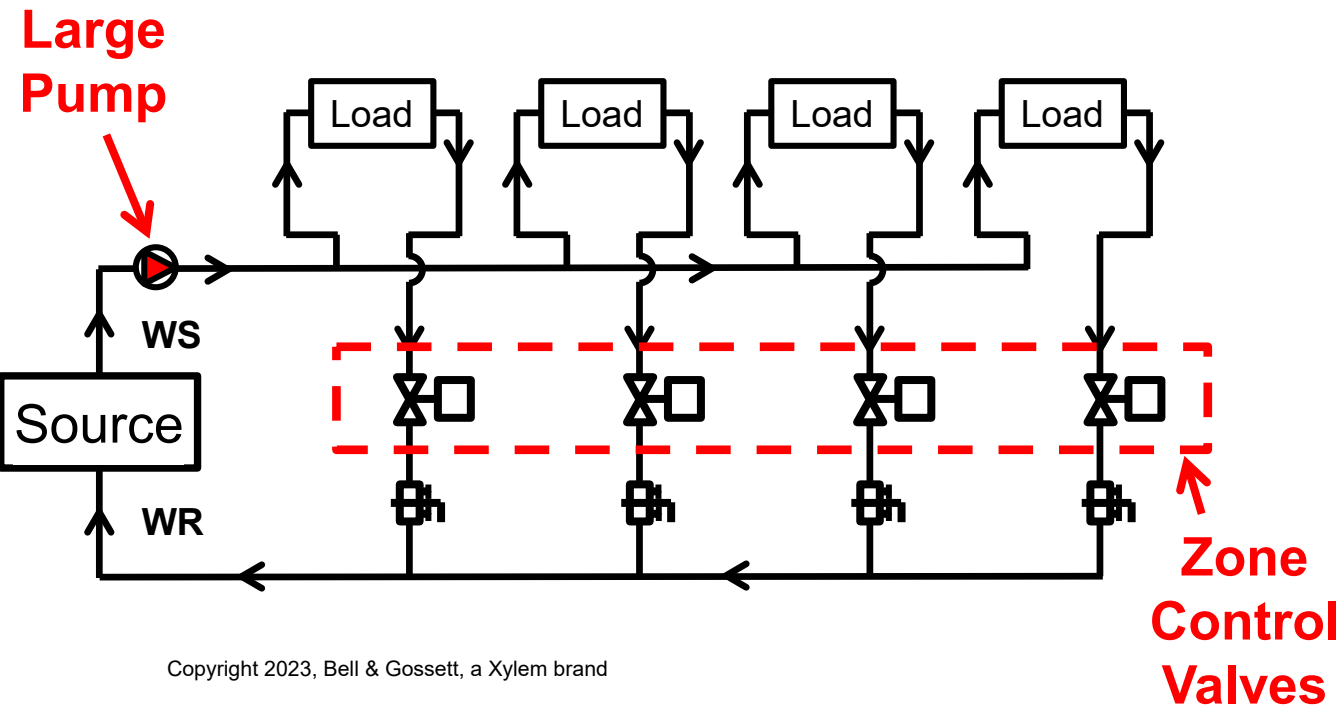


# Primary-Secondary - It's all about "The Pressure Drop"

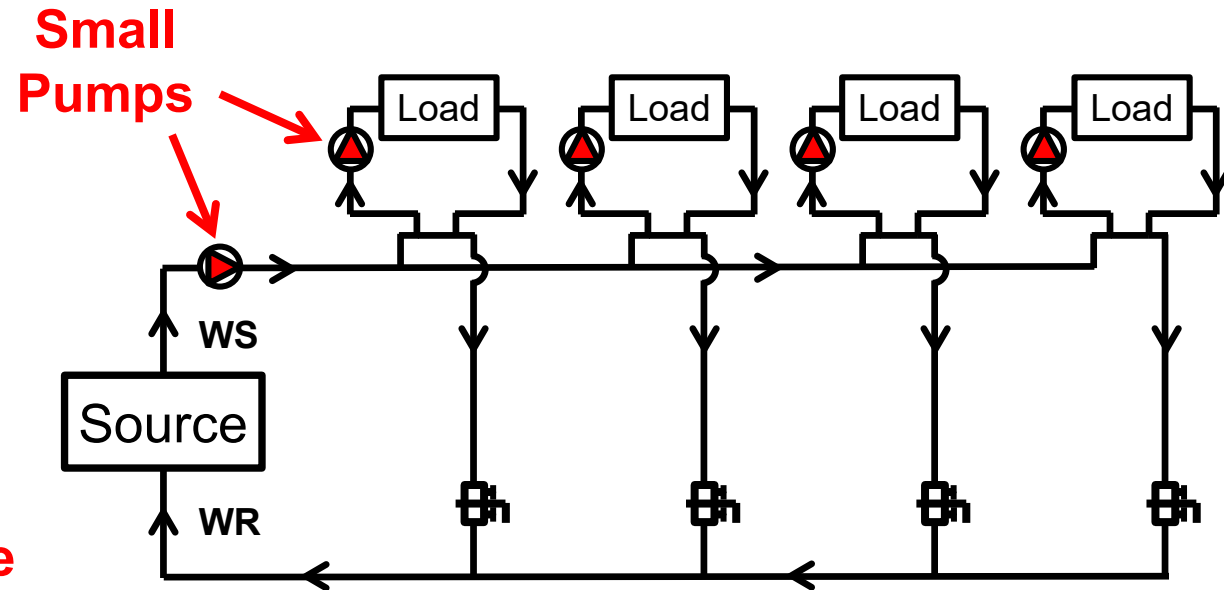
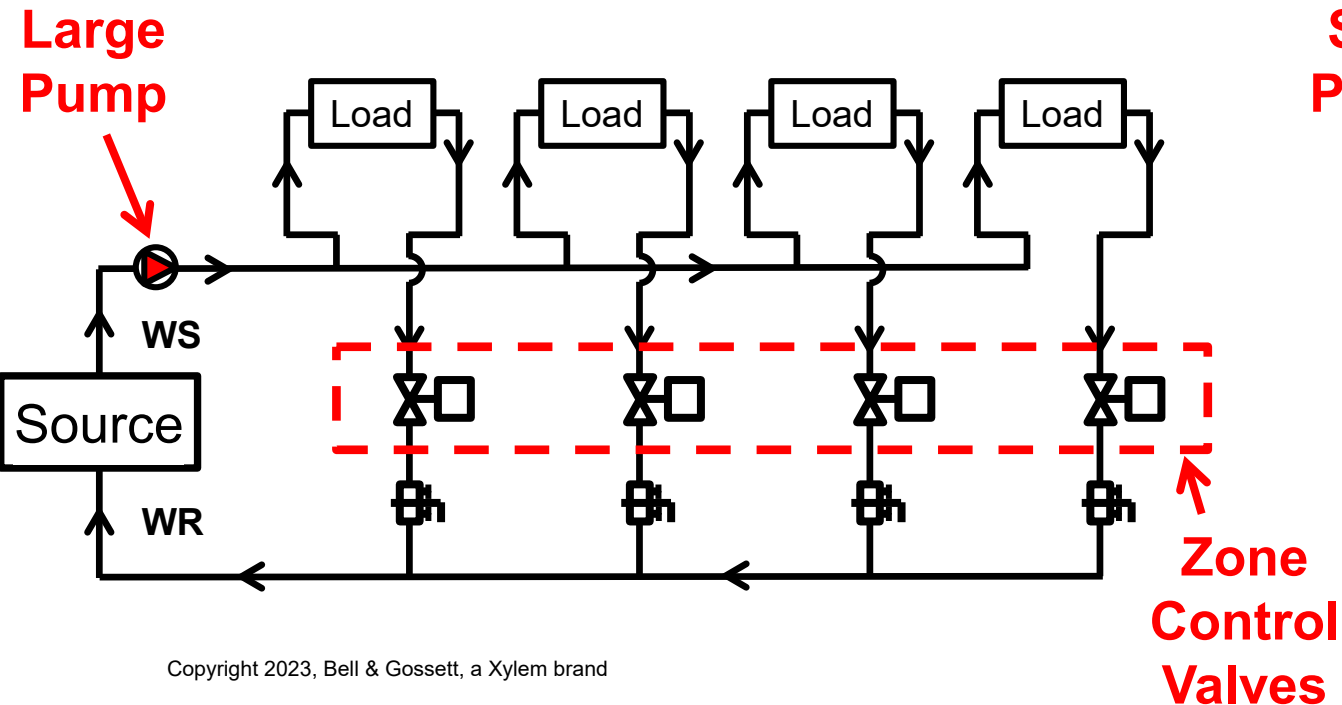


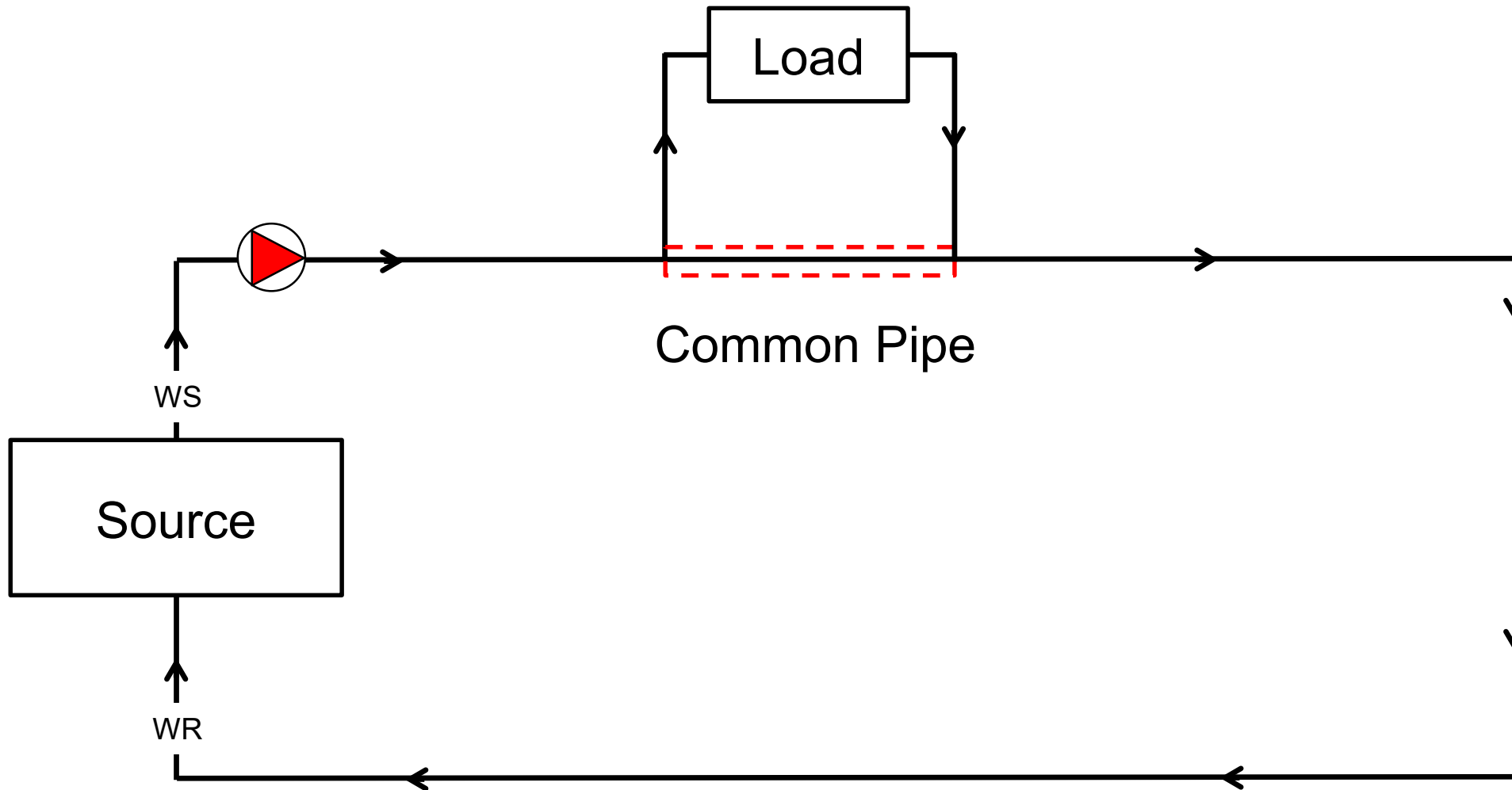


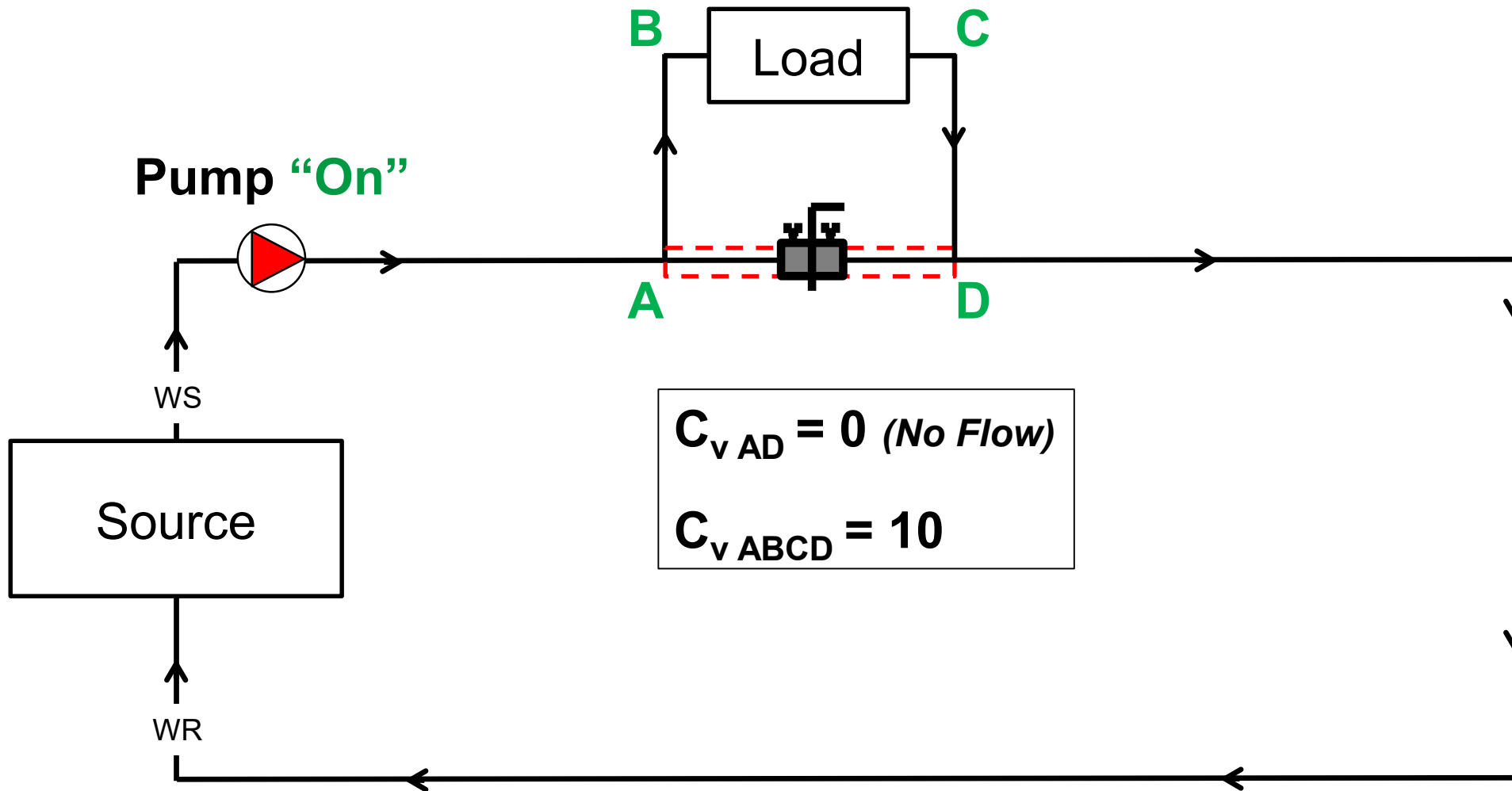
- Converts a Large Complex System into Smaller Manageable Sub-Systems



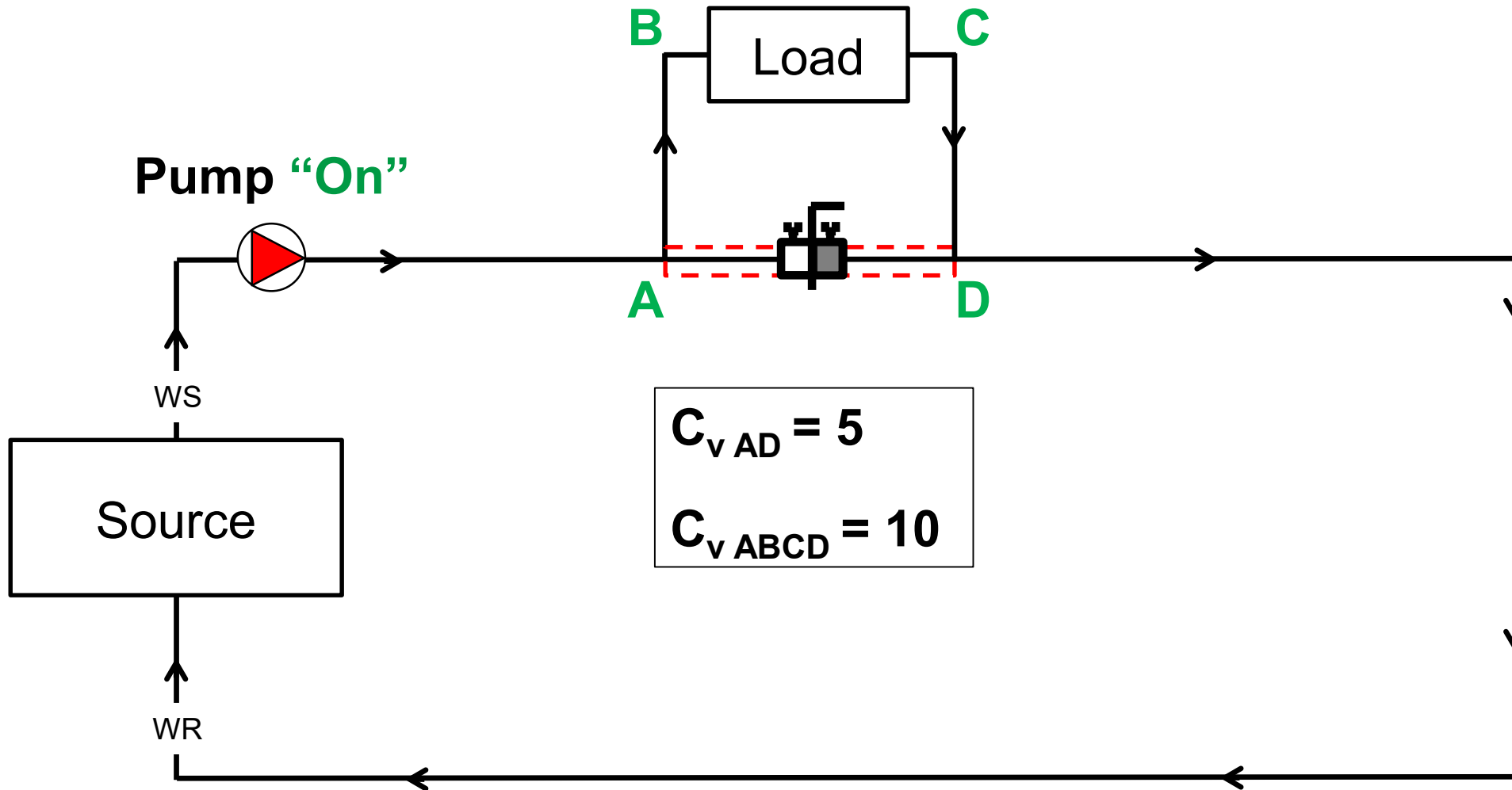
- Converts a Large Complex System into Smaller Manageable Sub-Systems
- Hydraulically Isolates One System from the Other
- Can Provide Thermal Separation







# Pressure Drop in Common Pipe – Valve 50% Closed

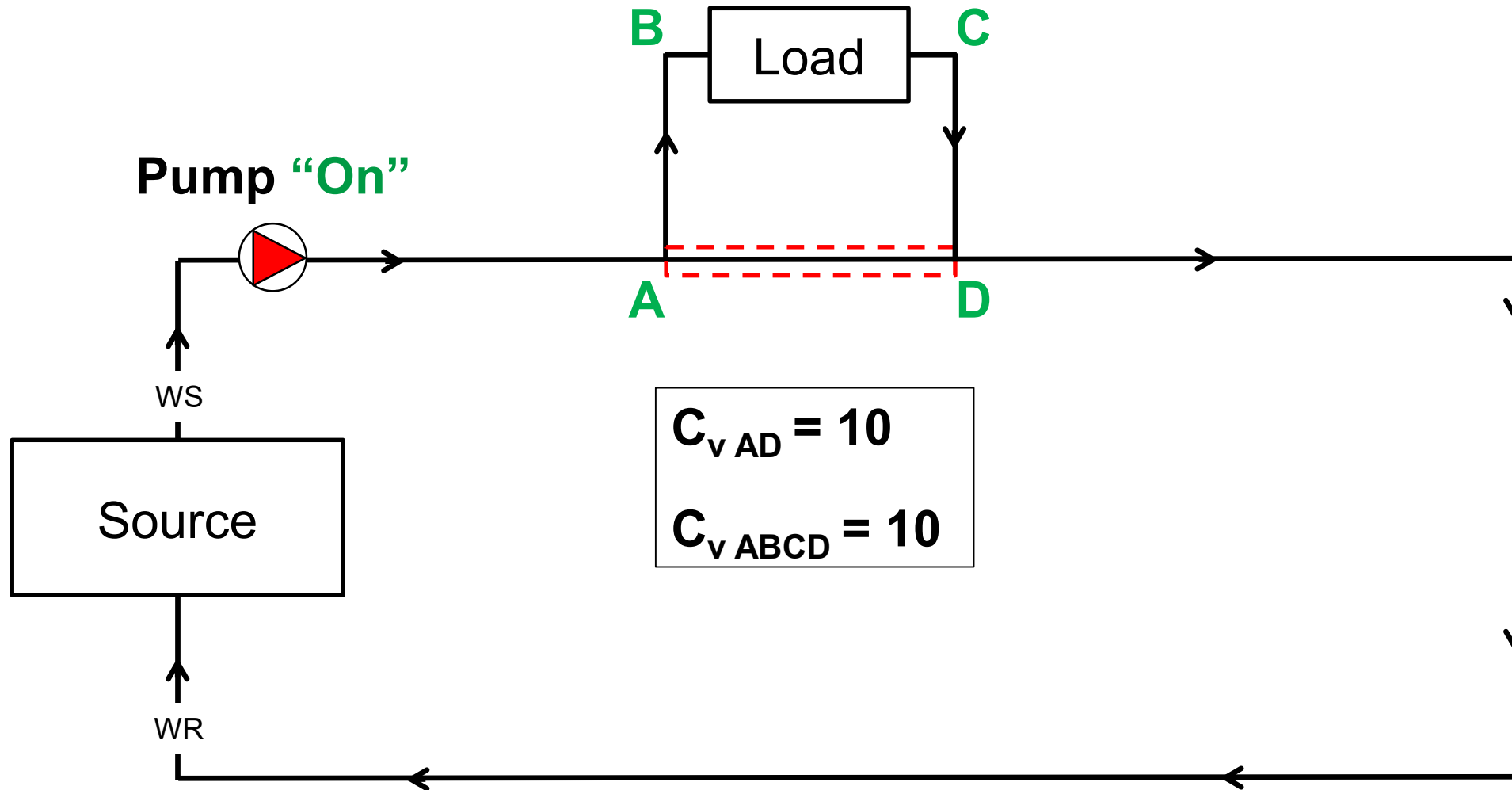


**C<sub>v</sub> Definition:** Flow, in **GPM**, Across an Open Valve when a Constant Pressure Differential of 1 PSI is Maintained.

$$C_v = \frac{Q}{\sqrt{\Delta P}}$$



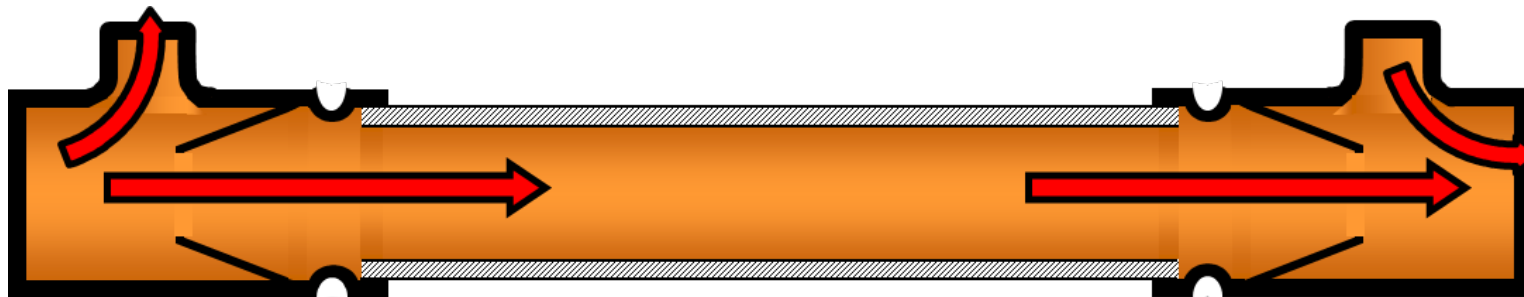
# Pressure Drop in Common Pipe – Valve Removed



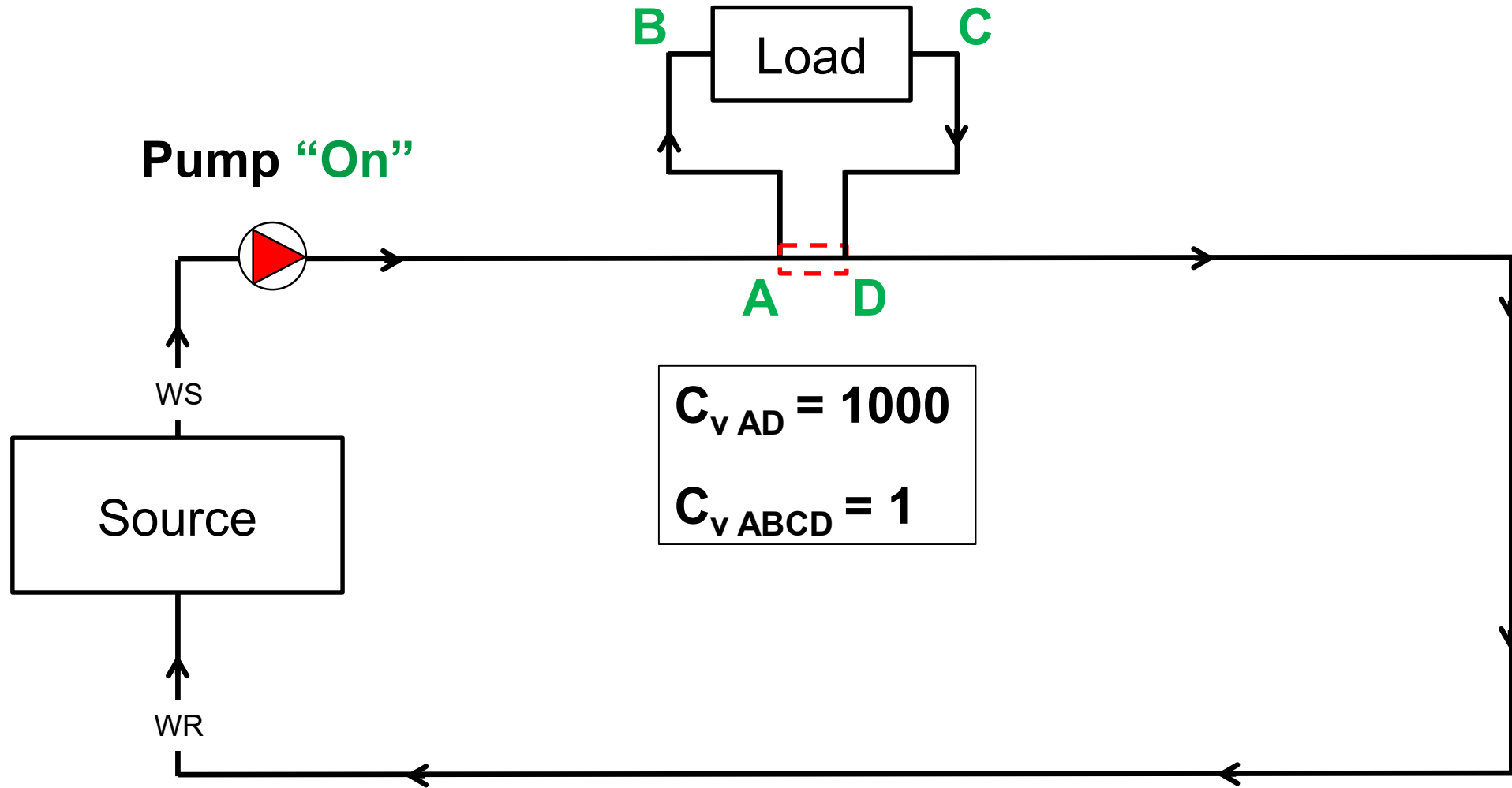
When Two Piping Circuits are Inter-Connected,

Flow in One Circuit Will Cause Flow in the Other,

**To a Degree**, Depending Upon the **Pressure Drop** in the Piping Common to Both.



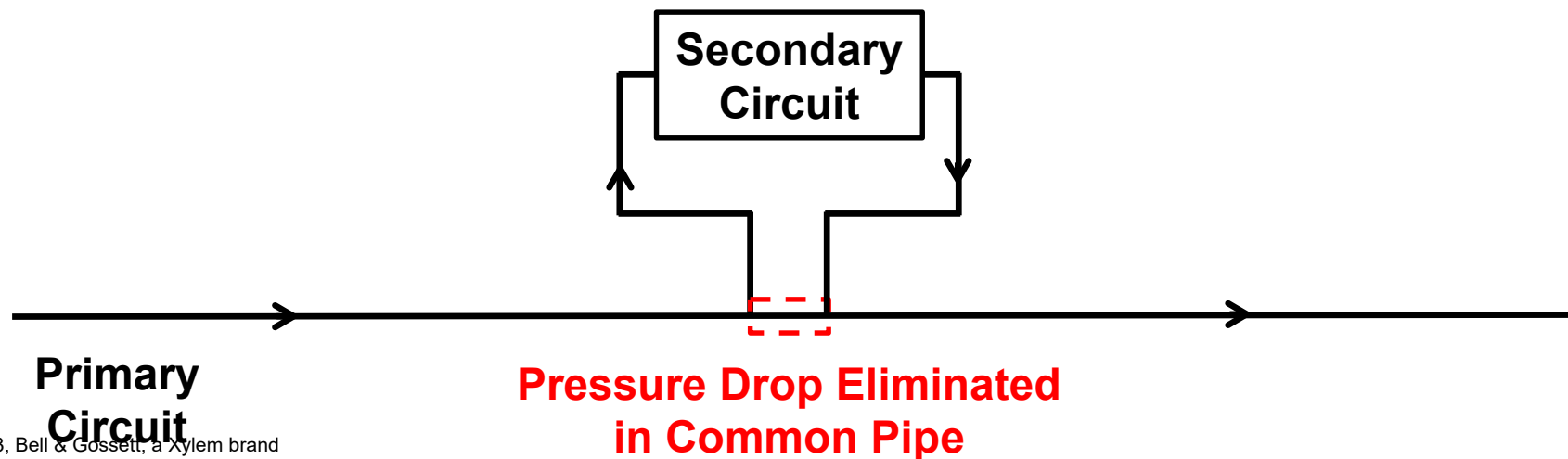
Common Pipe

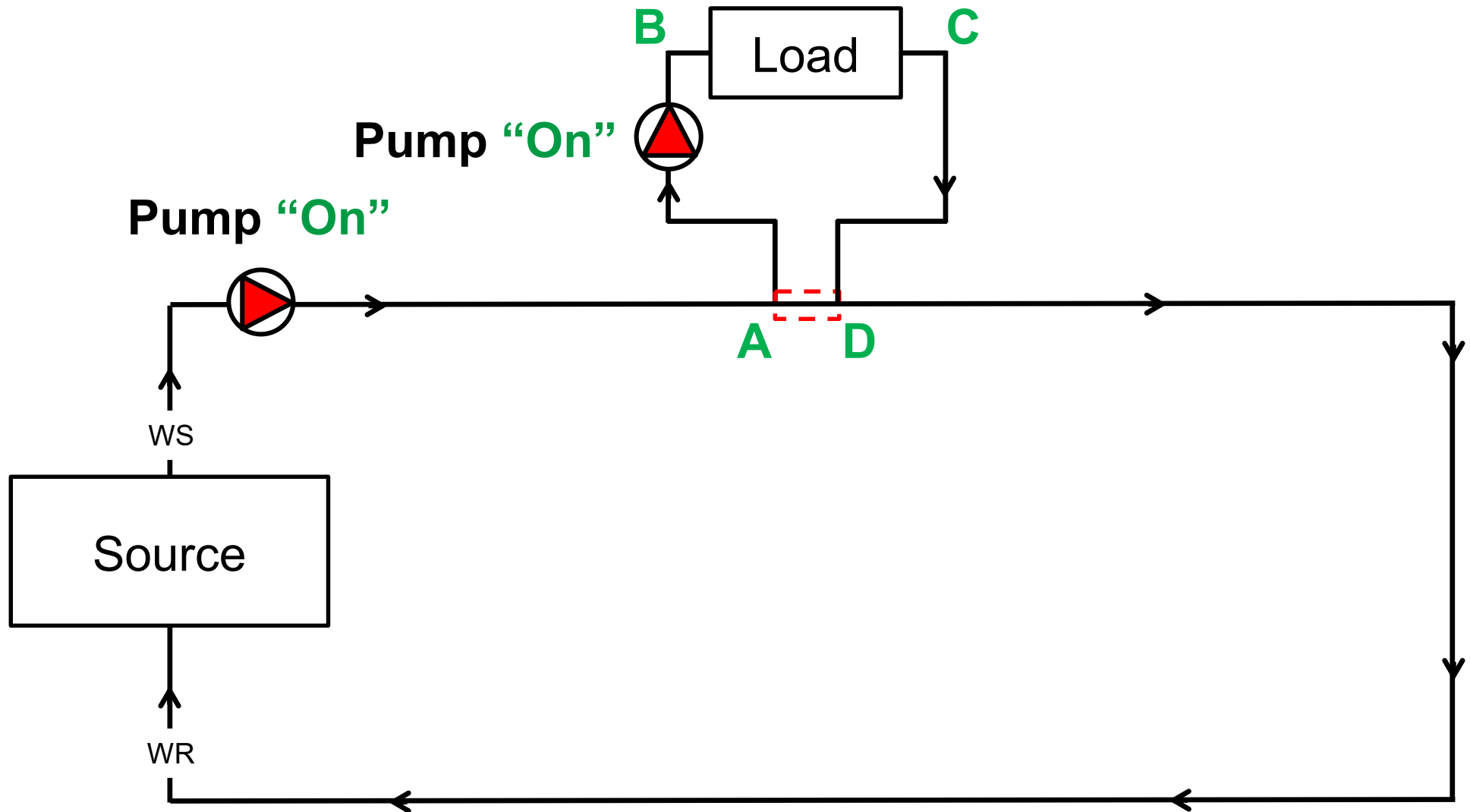


When Two Piping Circuits are Inter-Connected,

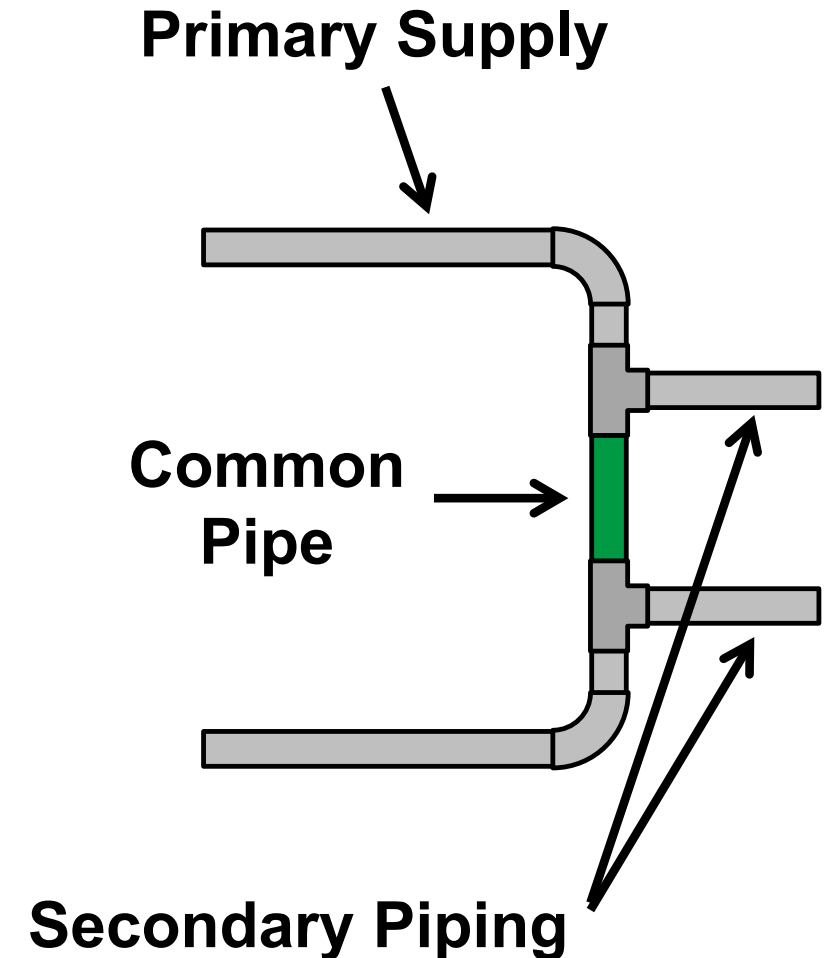
Flow in One Circuit Will **Not** Cause Flow in the Other,

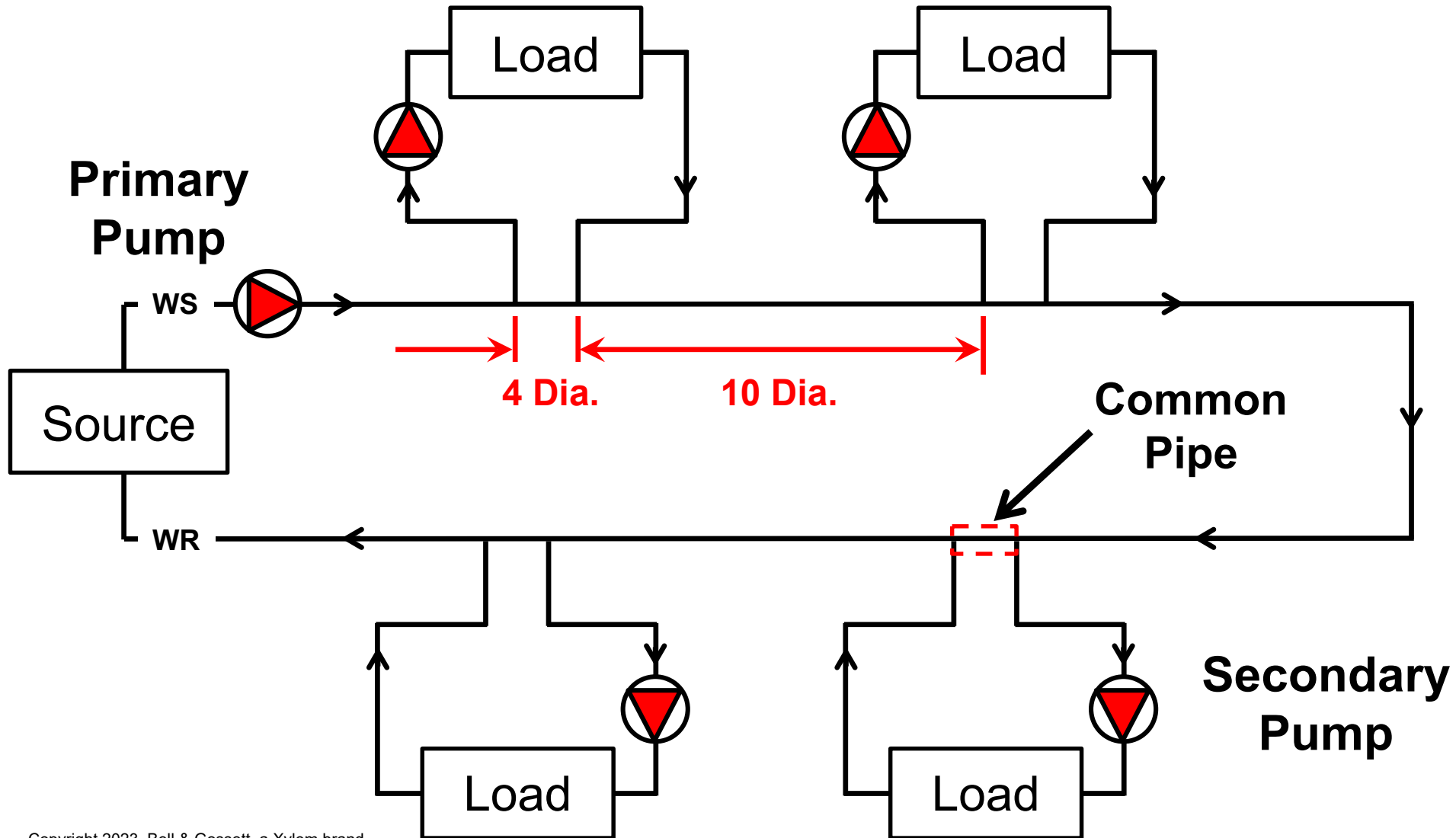
If the **Pressure Drop** in the Piping Common to Both is **Eliminated**.



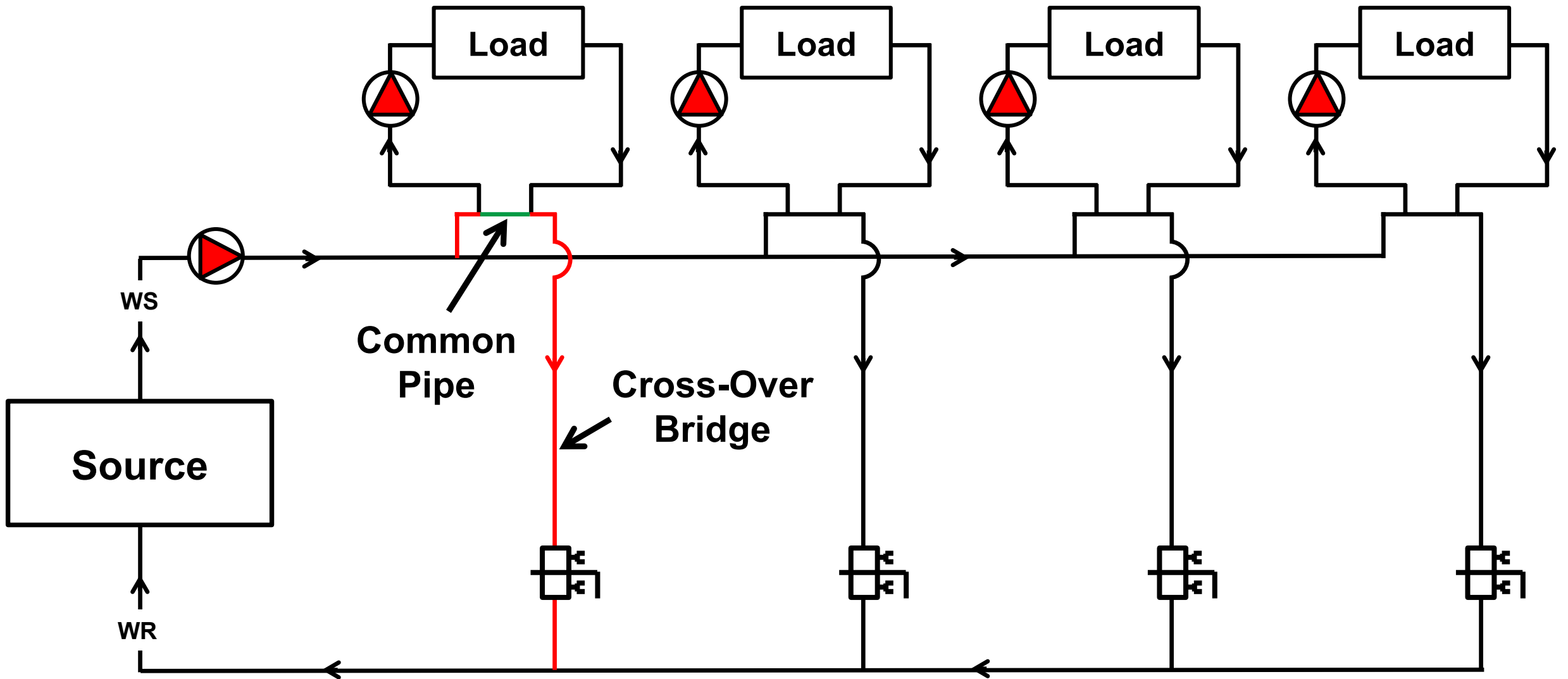


- Three to Four Pipe Diameters Between Tees  
*(Recommend no less than 12")*
- Head Loss Less Than **1.5 Feet**  
*(Recommend size equal to Primary Supply)*
- Keep Velocities Low in Secondary Piping  
*(Recommend 2-4 FPS for air control and noise)*



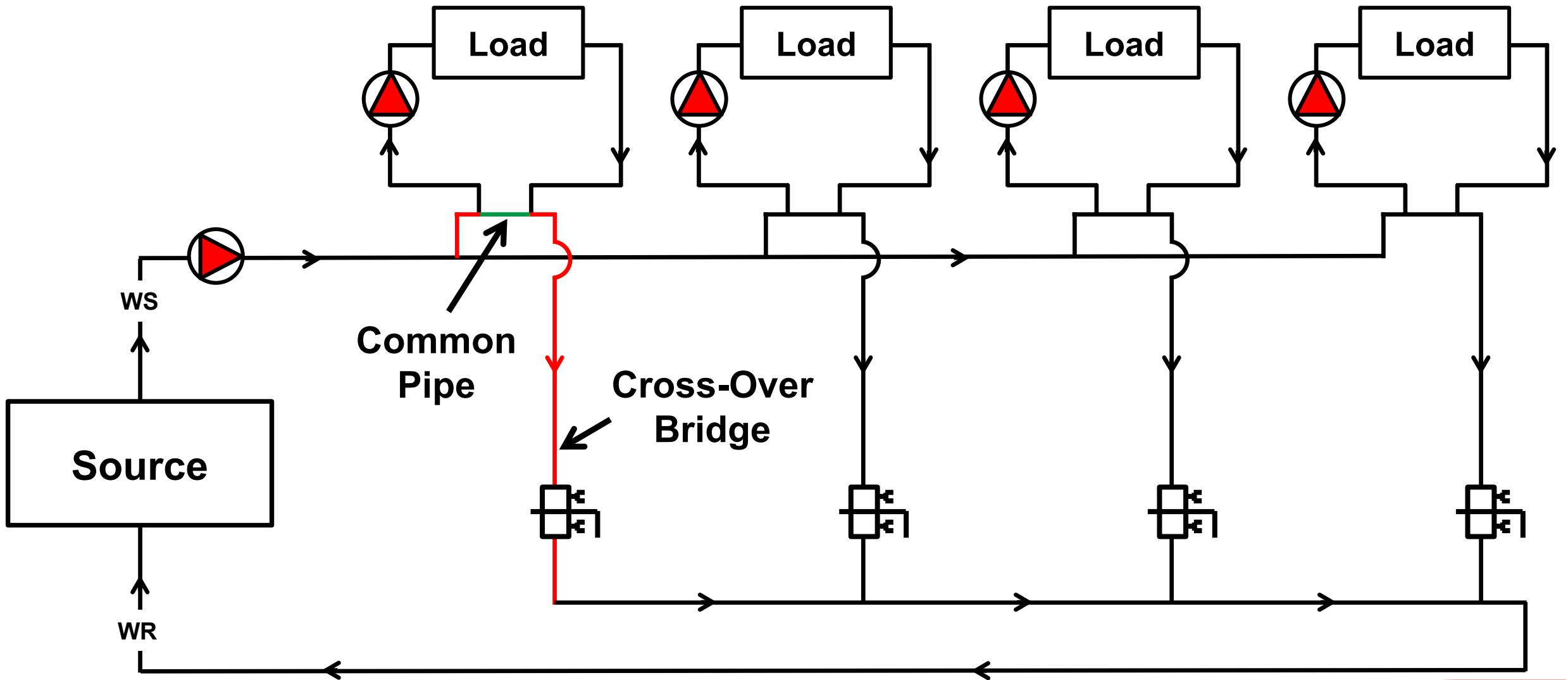


# Primary-Secondary System

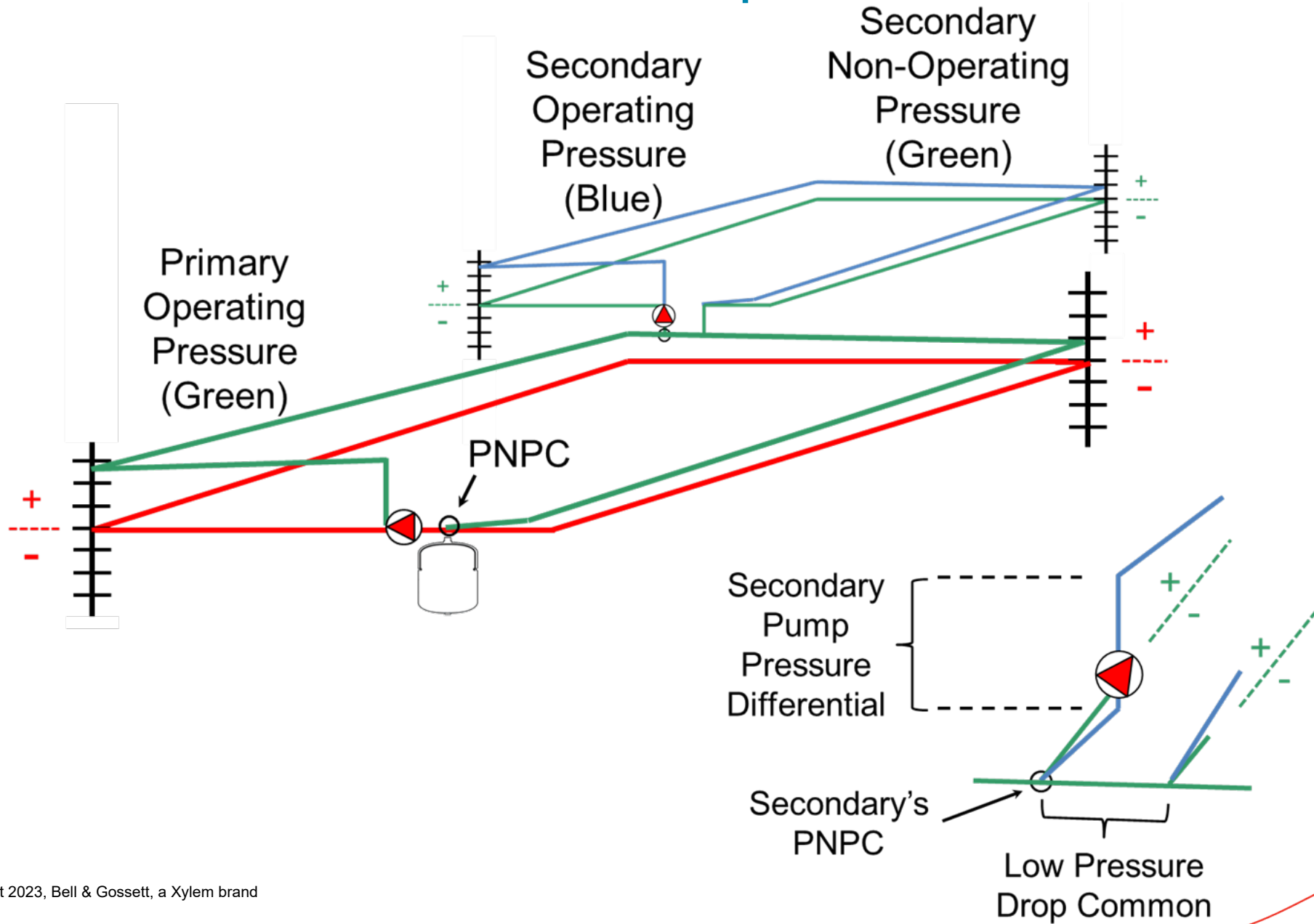




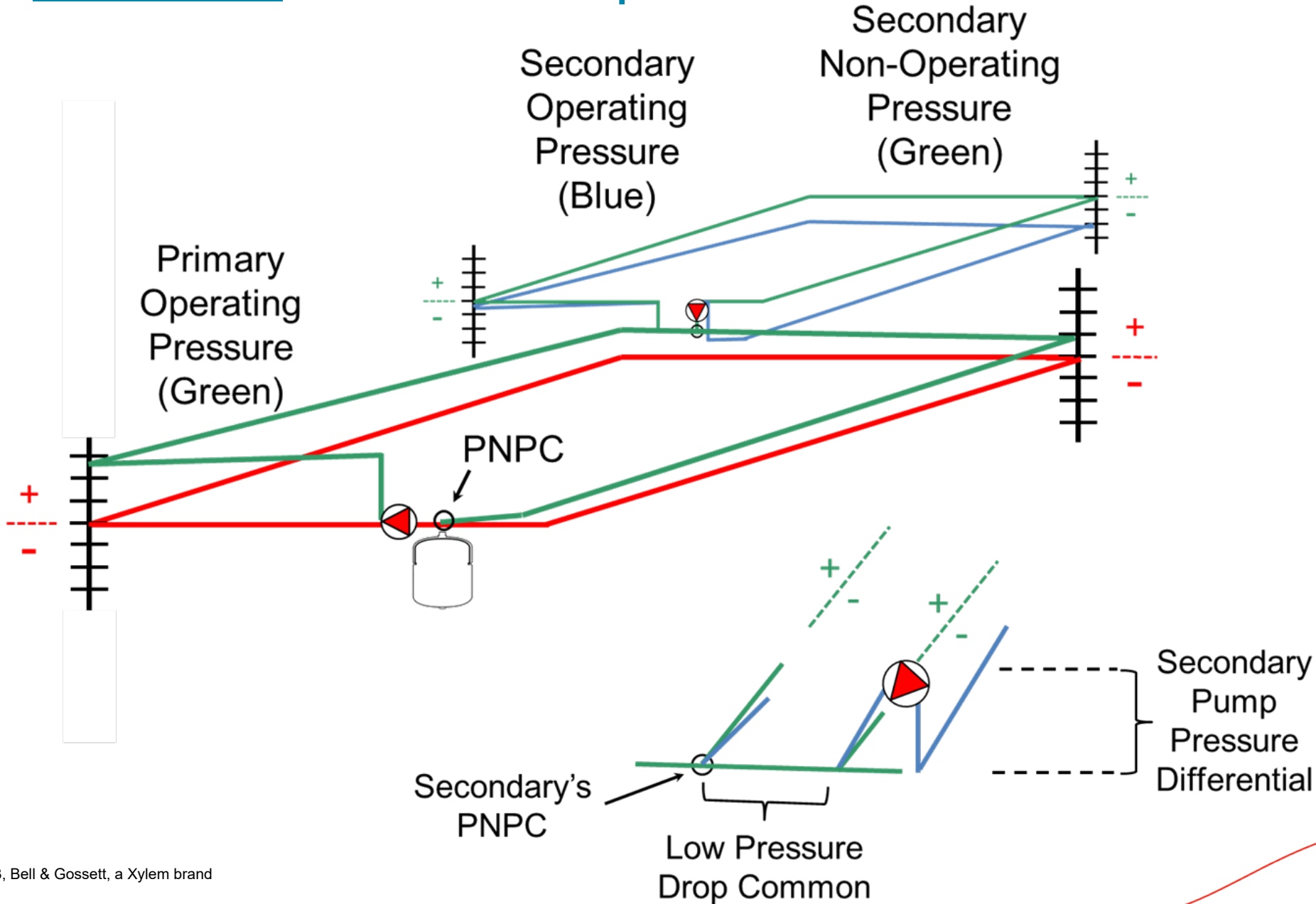
# Primary-Secondary System

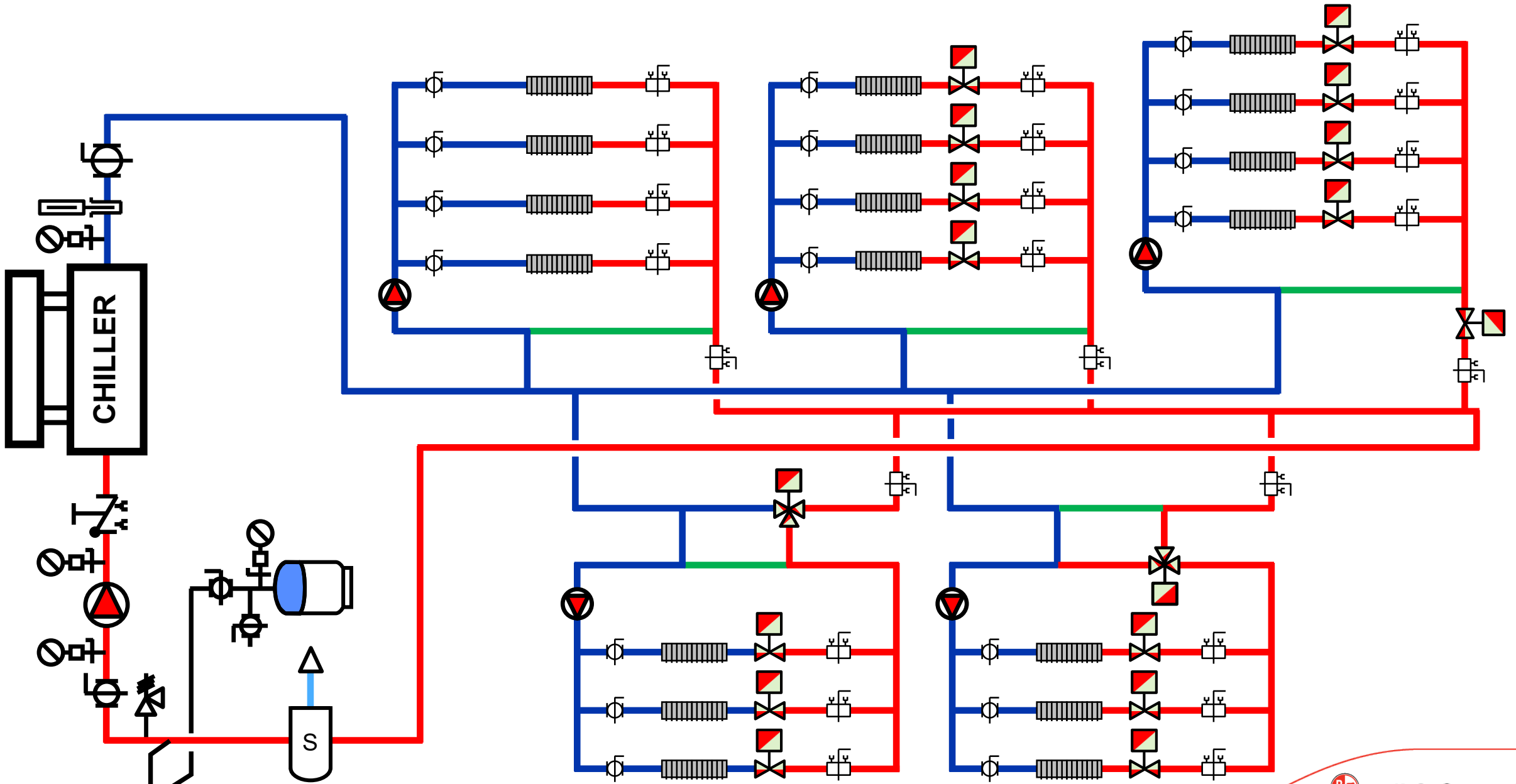


# From Common Pipe

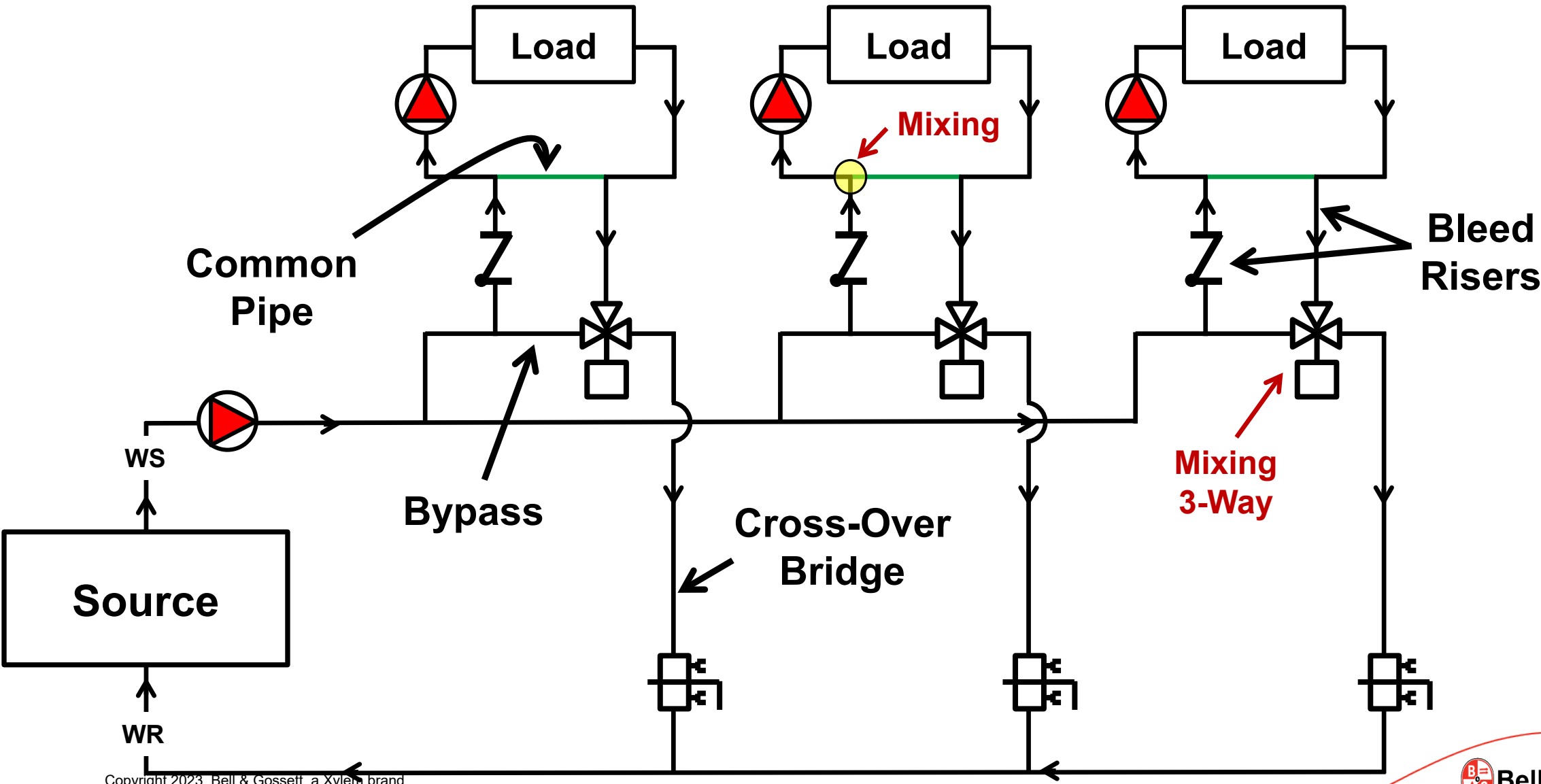


# Common Pipe

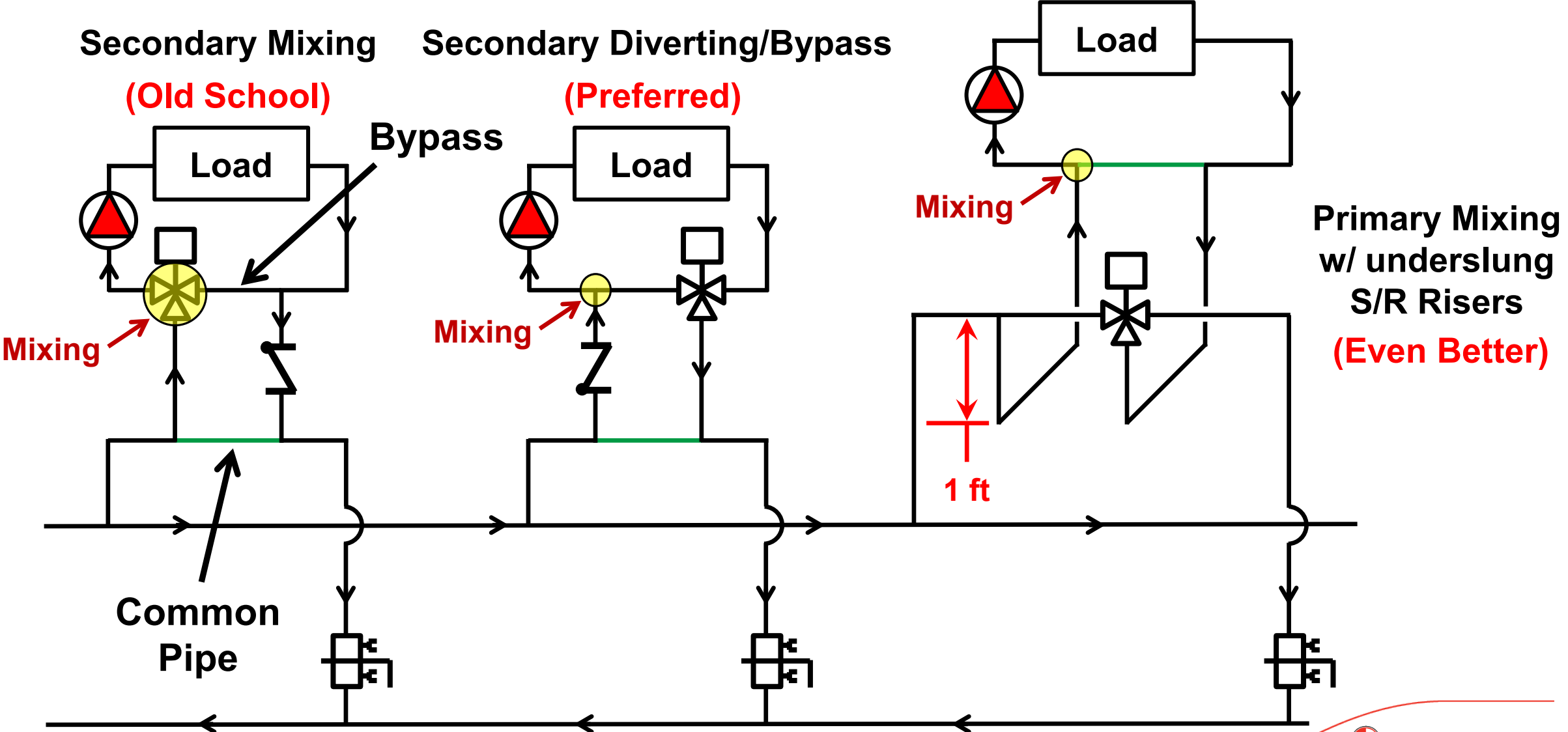




# Continuous Secondary Pump Circulation

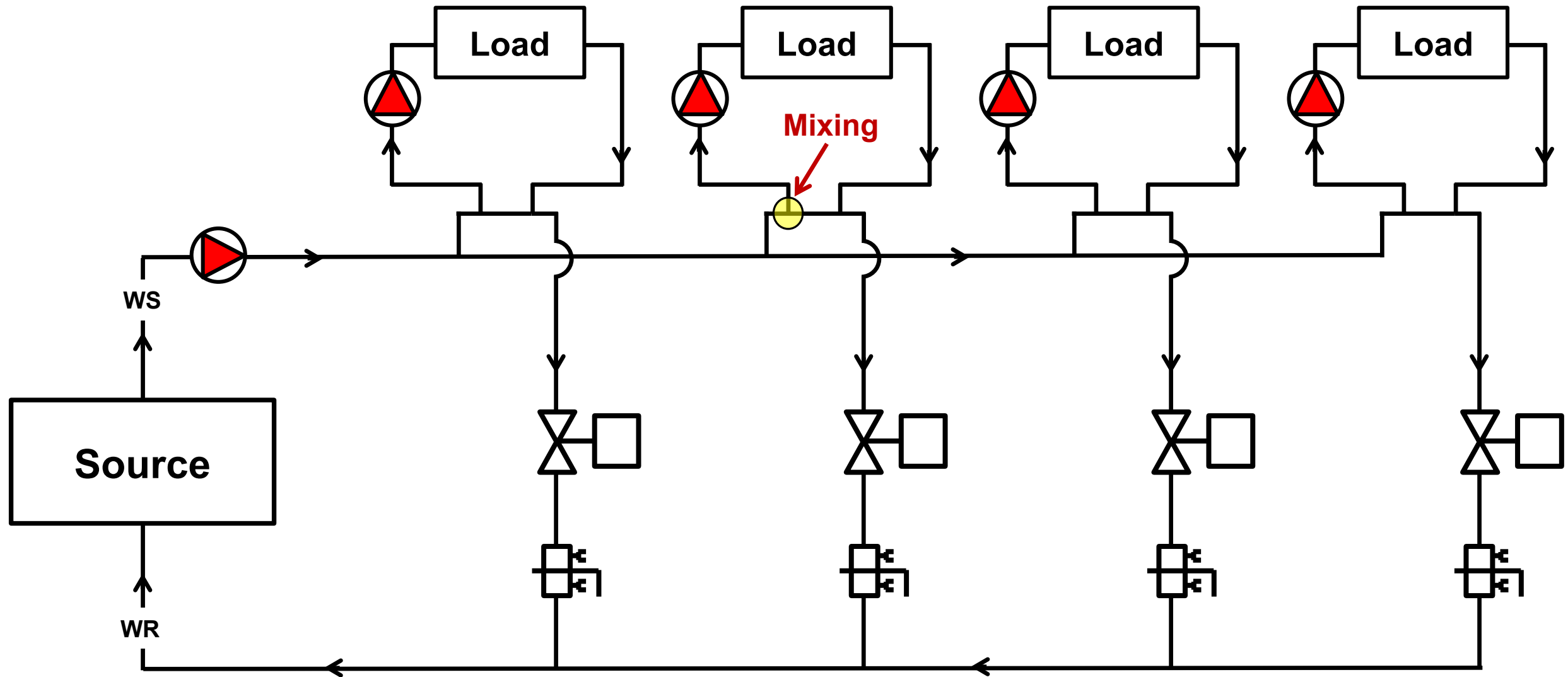


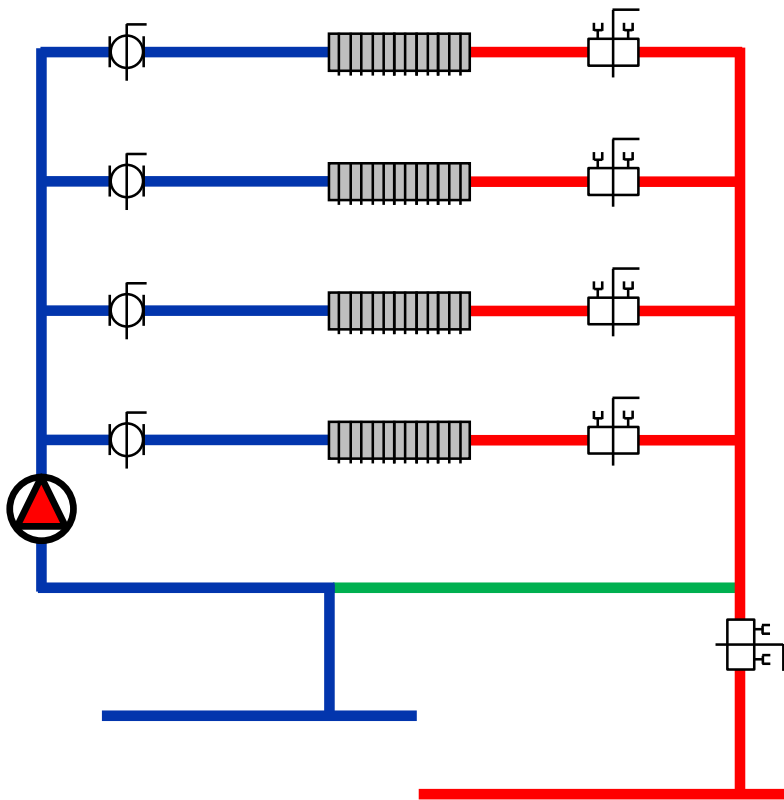
# Continuous Secondary Pump Circulation



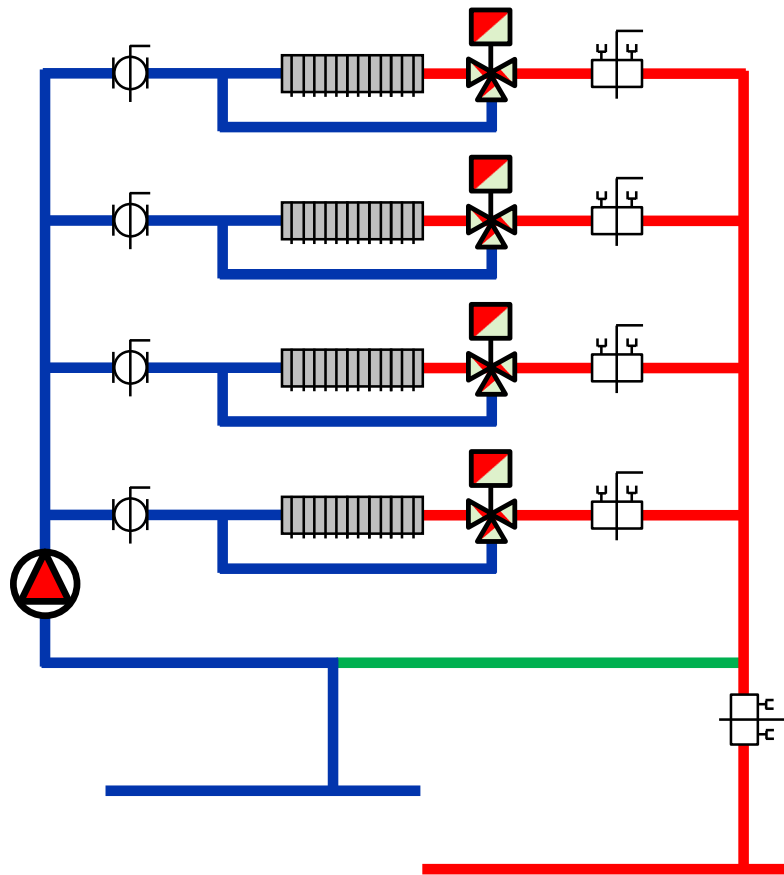
# Primary-Secondary Modulating 2-Way Valve Control

**Source Pump Variable Speed Control possible**

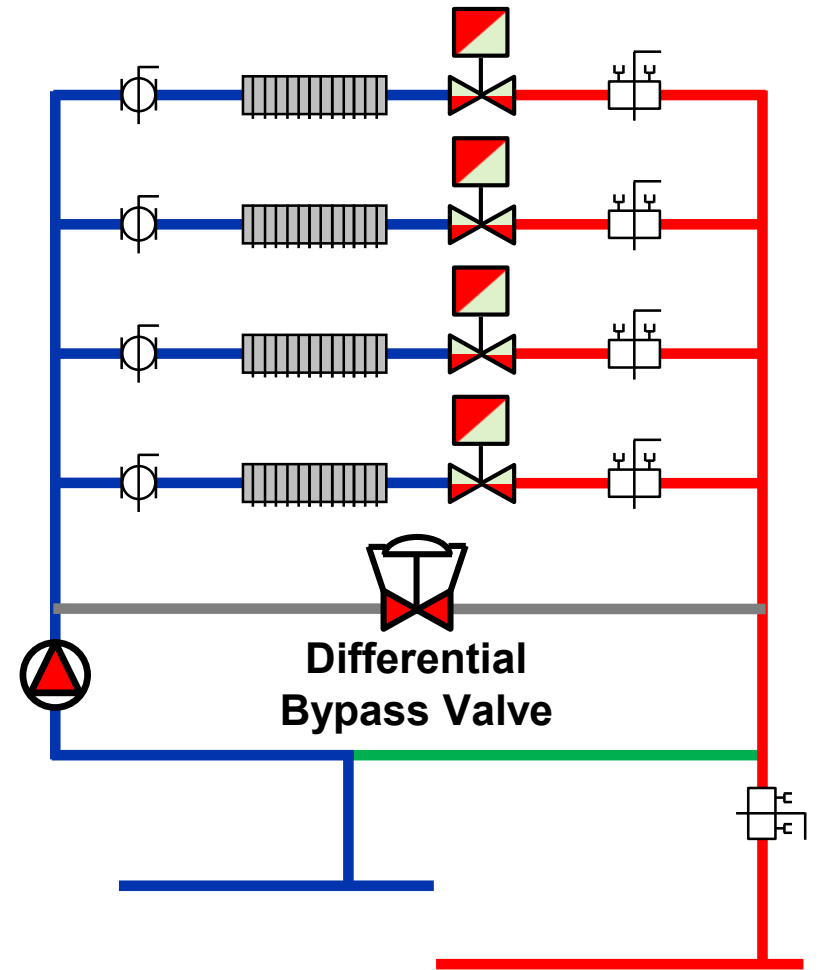




**Constant Secondary Flow  
("On/Off" Pump Control)**

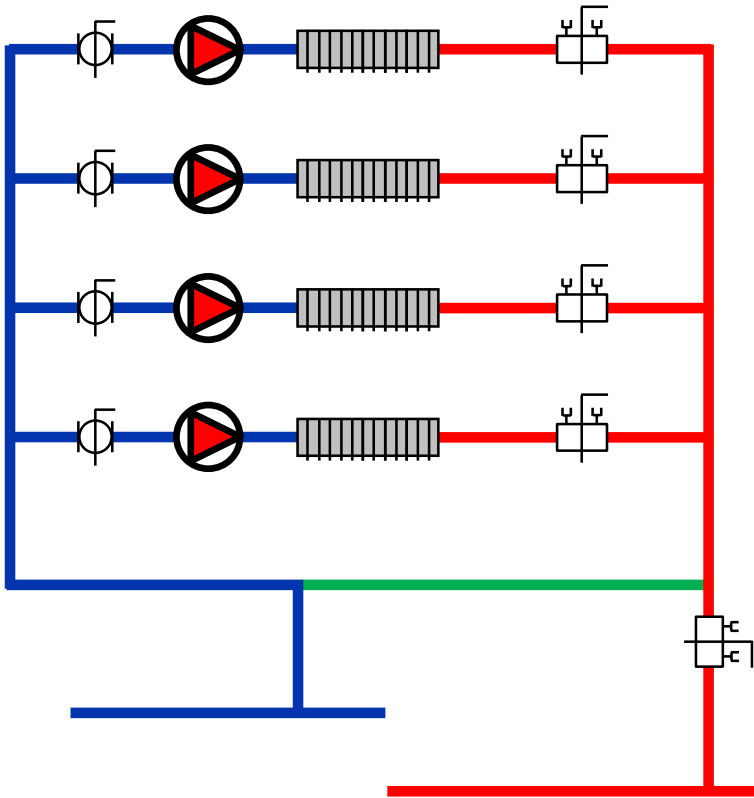


**Constant Secondary Flow  
(Continuous Pump)**

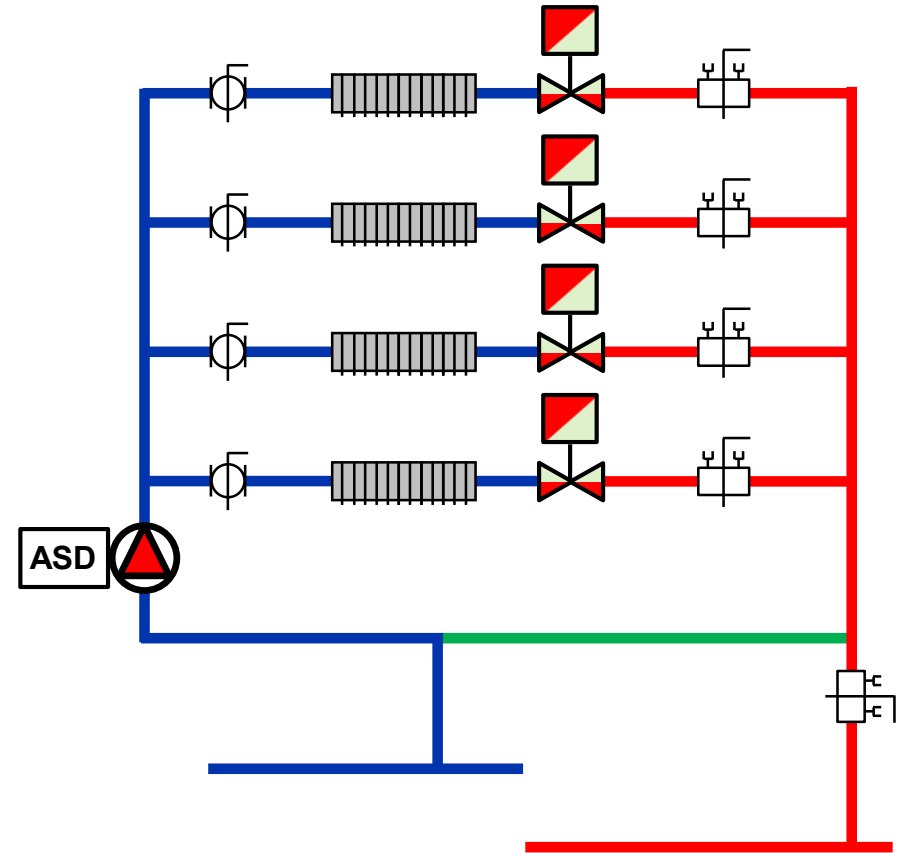


**Variable Secondary Flow  
(Continuous Pump)**



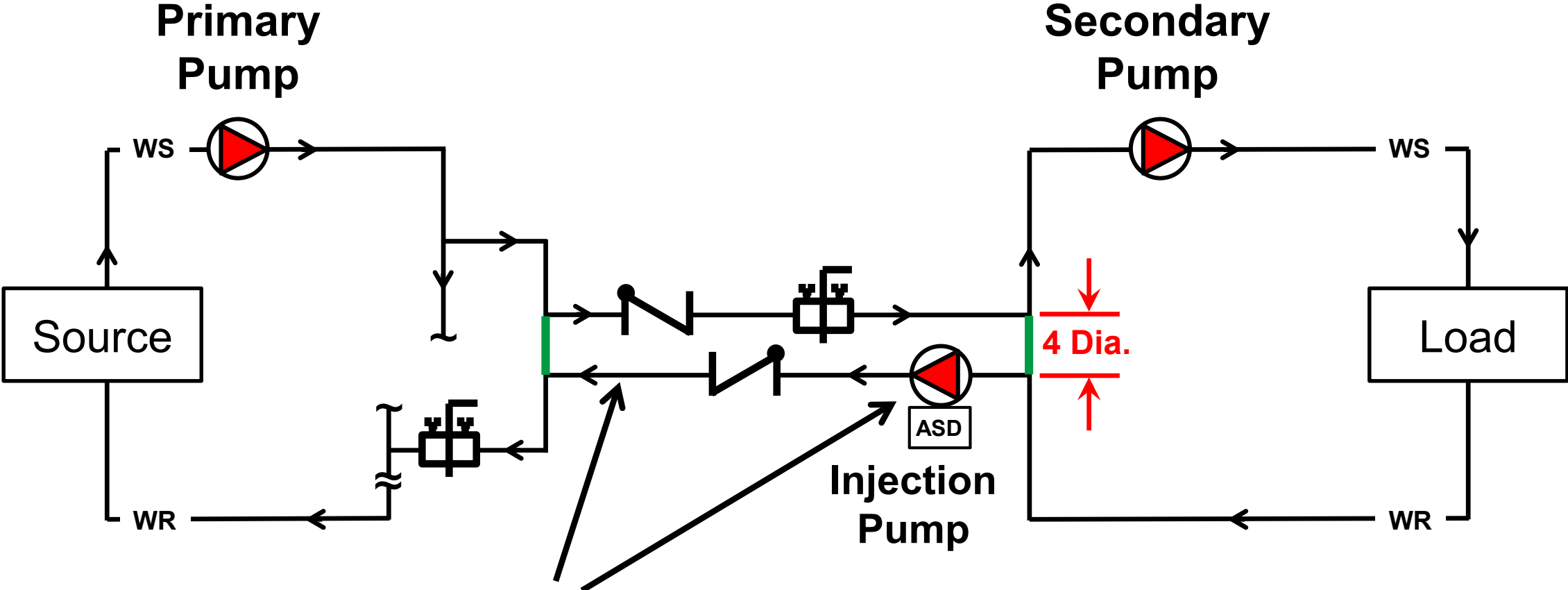


**Constant Secondary Flow  
("On/Off" Constant Speed)  
(Integrated Variable Speed)**



**Variable Secondary Flow  
(Variable Speed Pump)**

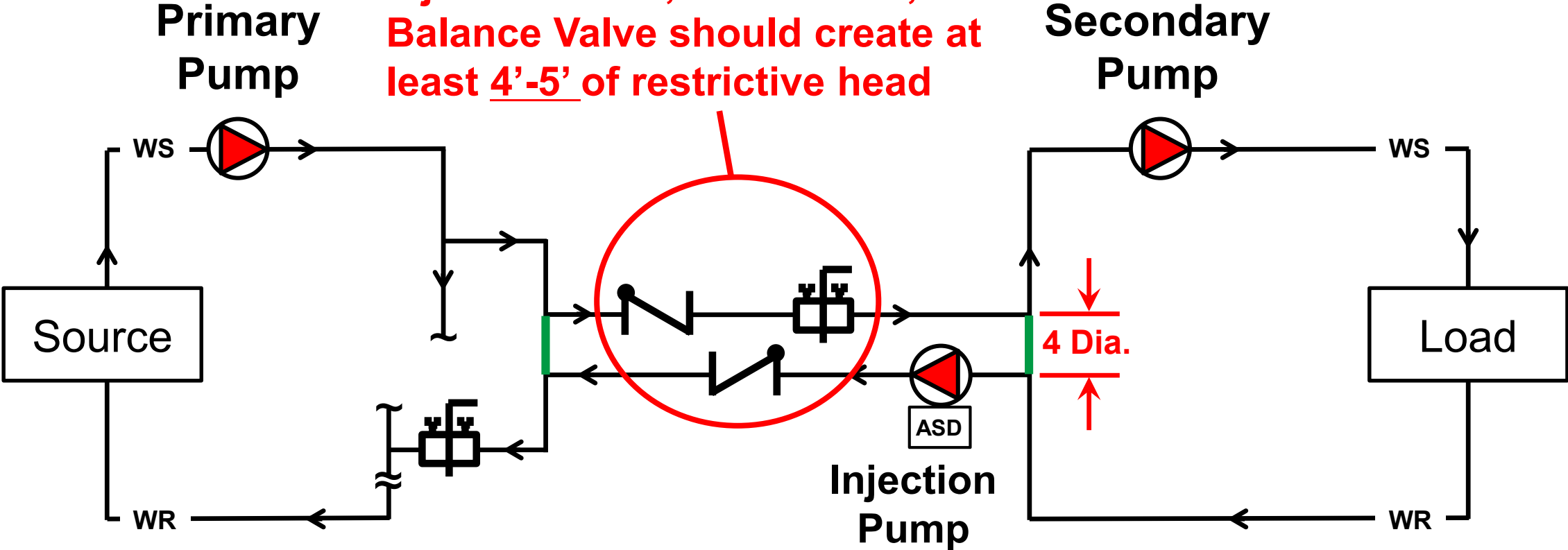
# From a Cross-Over Bridge



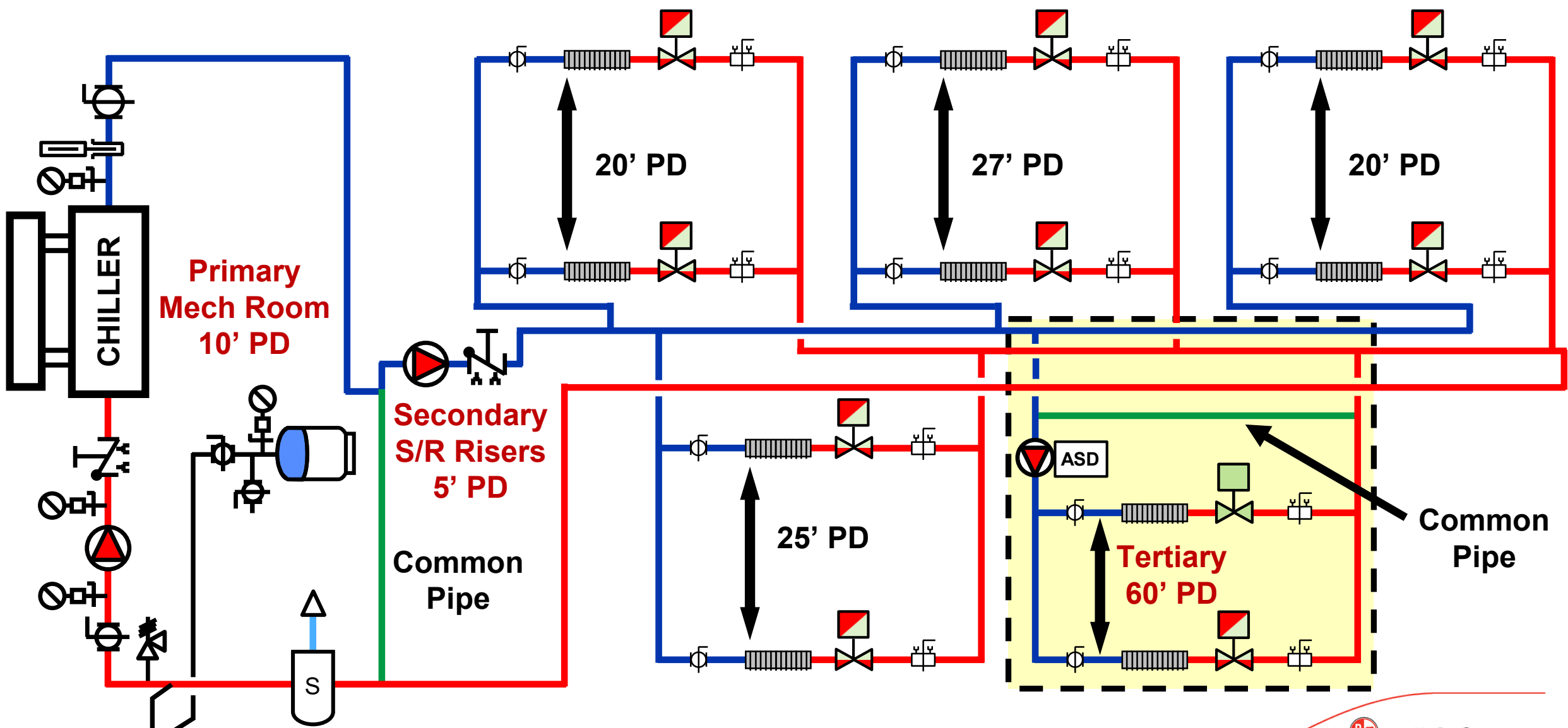
**Injection Risers and Pump sized to Full Load Primary Cross-Over Flow**

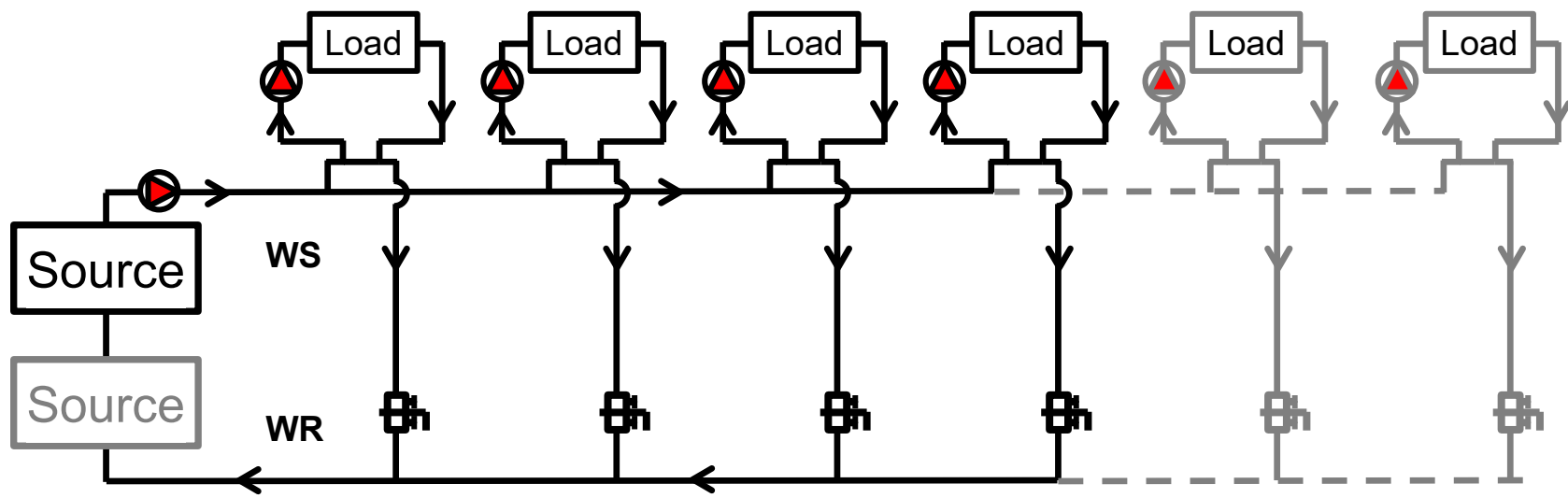
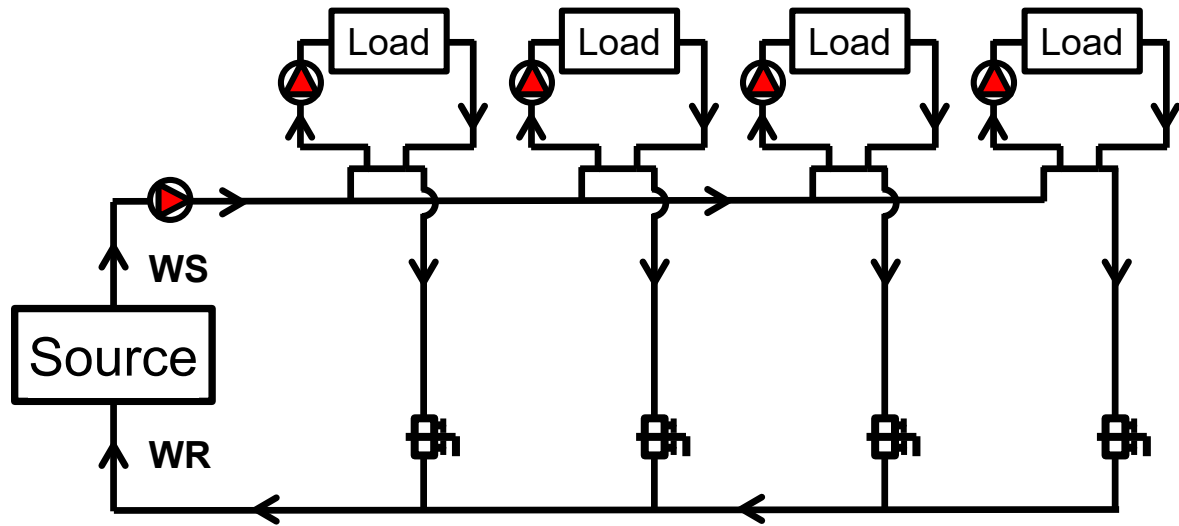
# From a Cross-Over Bridge

**Injection Riser, Flo-Control, and Balance Valve should create at least 4'-5' of restrictive head**



\_\_\_\_\_?

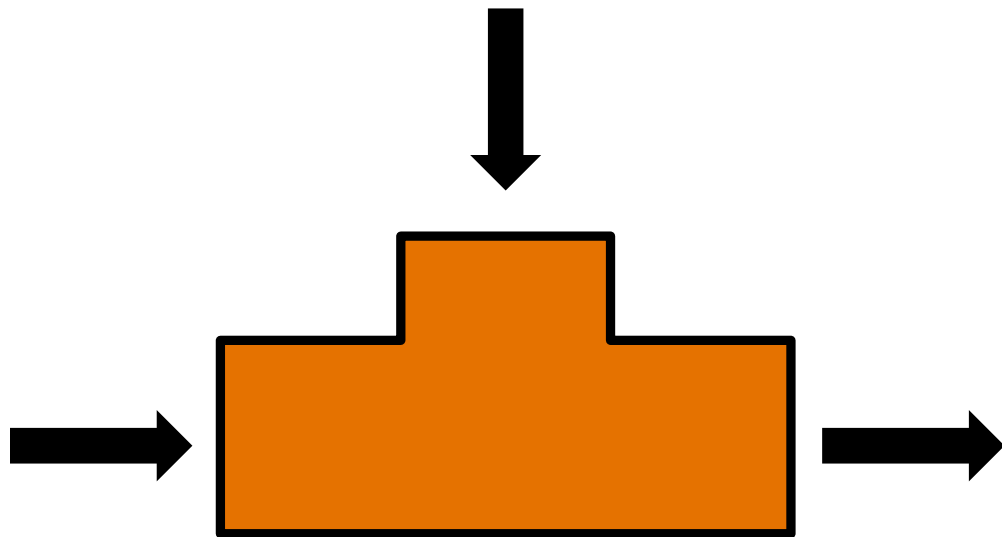




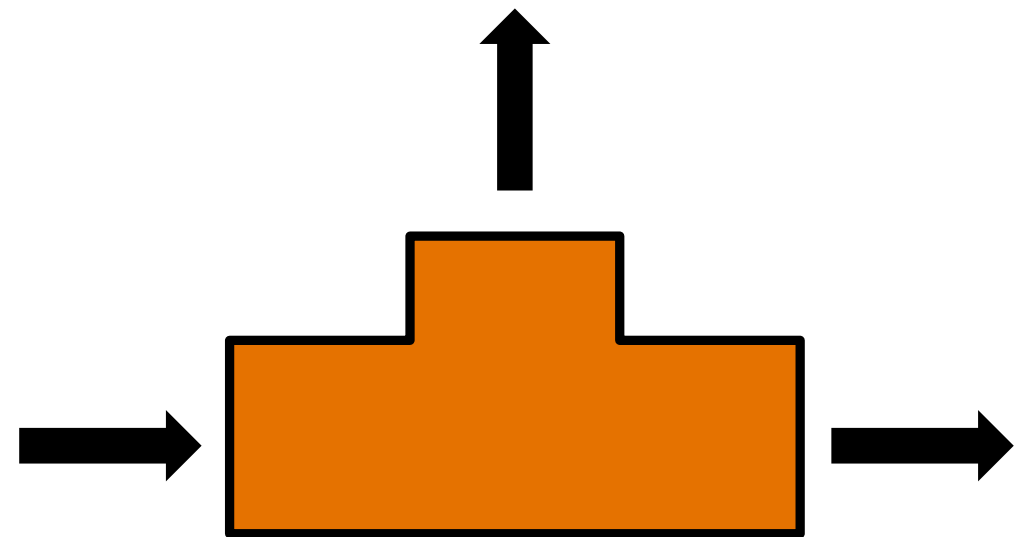
Remember – It's the Law!

The Flow Rate (GPM) Entering a Tee.....

Must Equal the Flow Rate Leaving the Tee!

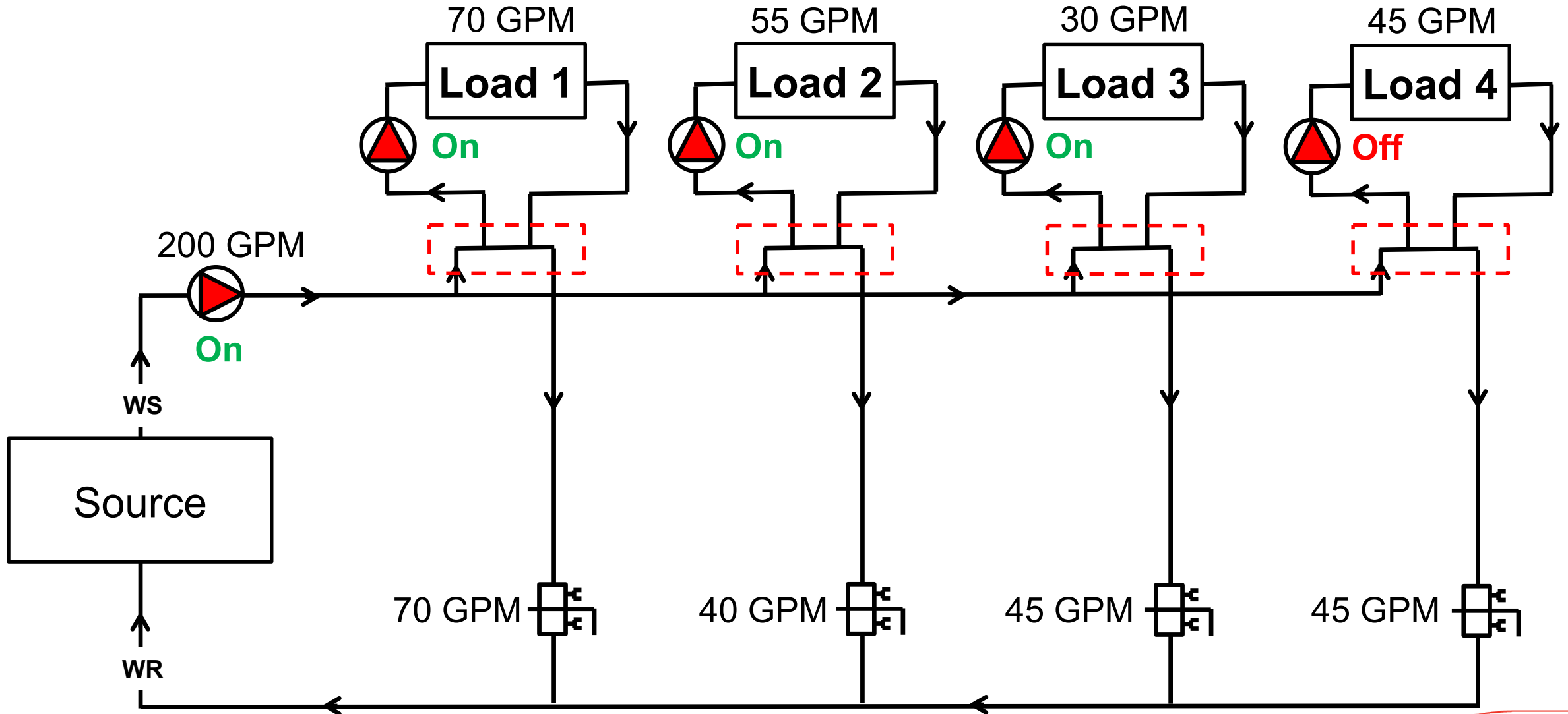


Mixing Tee



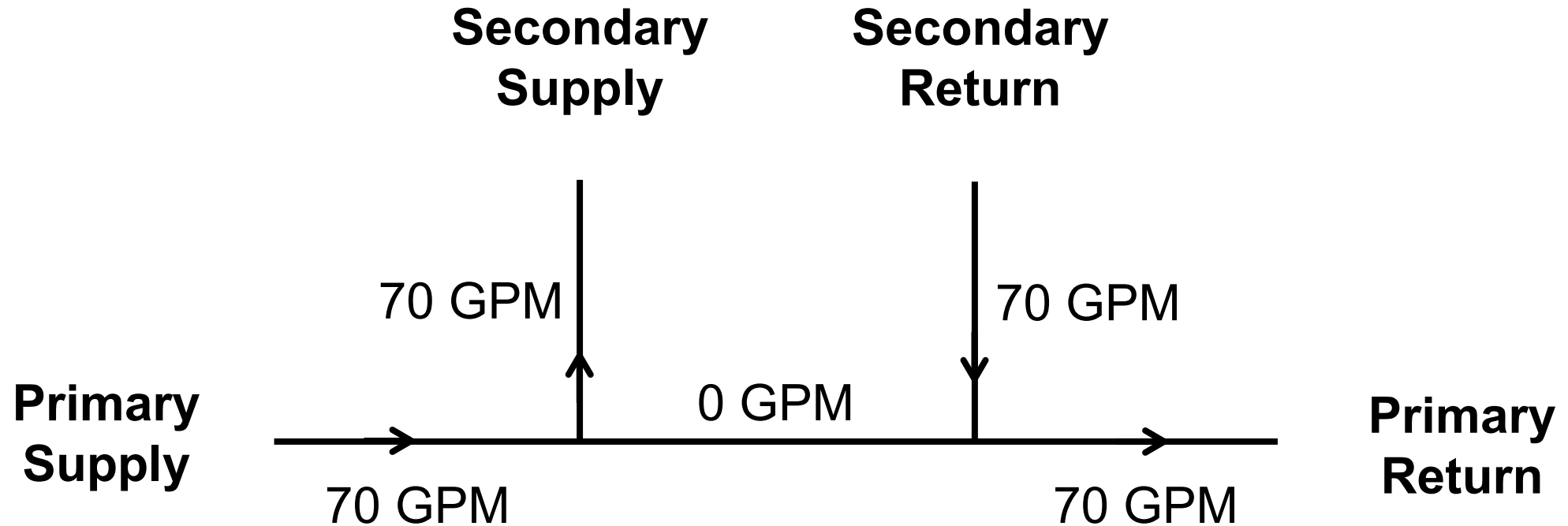
Diverting Tee

# Primary-Secondary Flow Rates



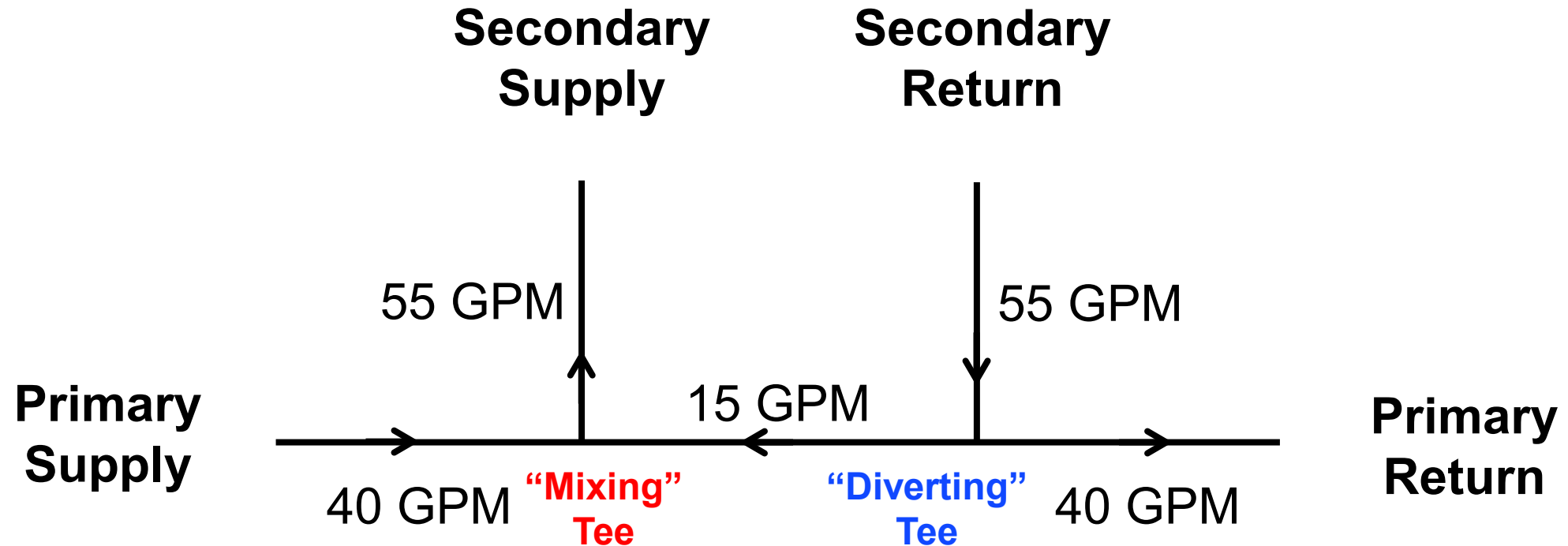


# \_\_\_\_\_ to Secondary Flow



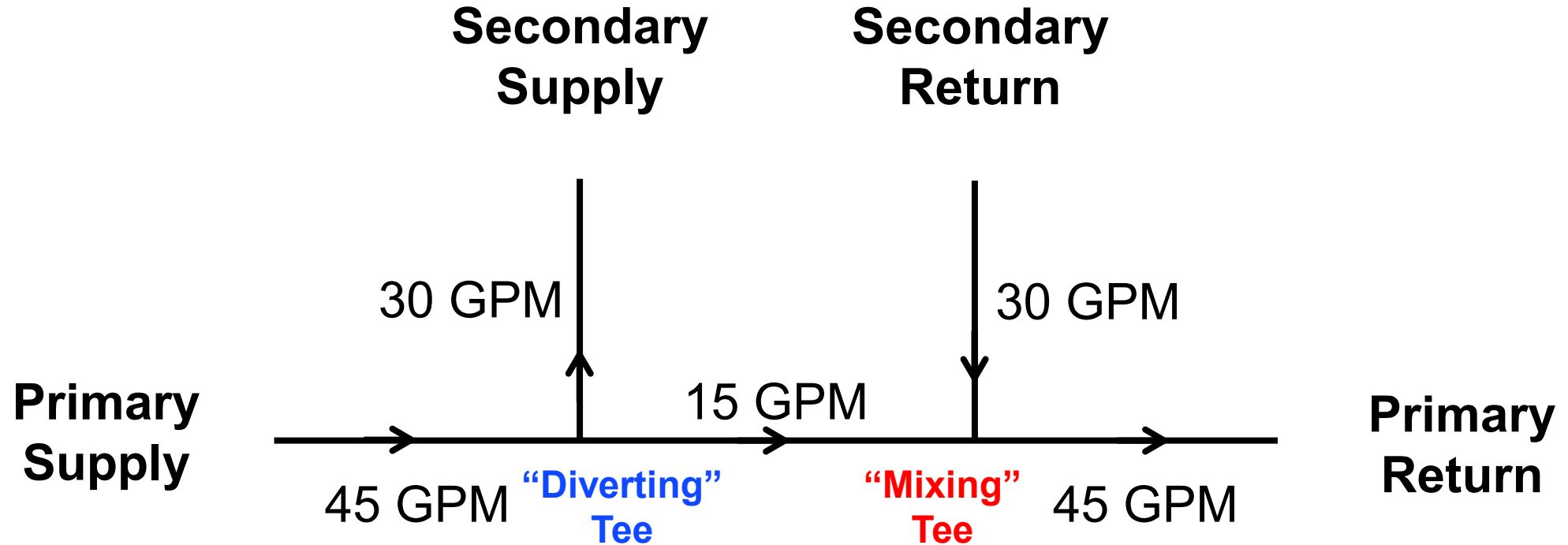
- No Flow in the Common Pipe
- Secondary Supply Temp = Primary Supply Temp
- Primary Return Temp = Secondary Return Temp

# Secondary Flow



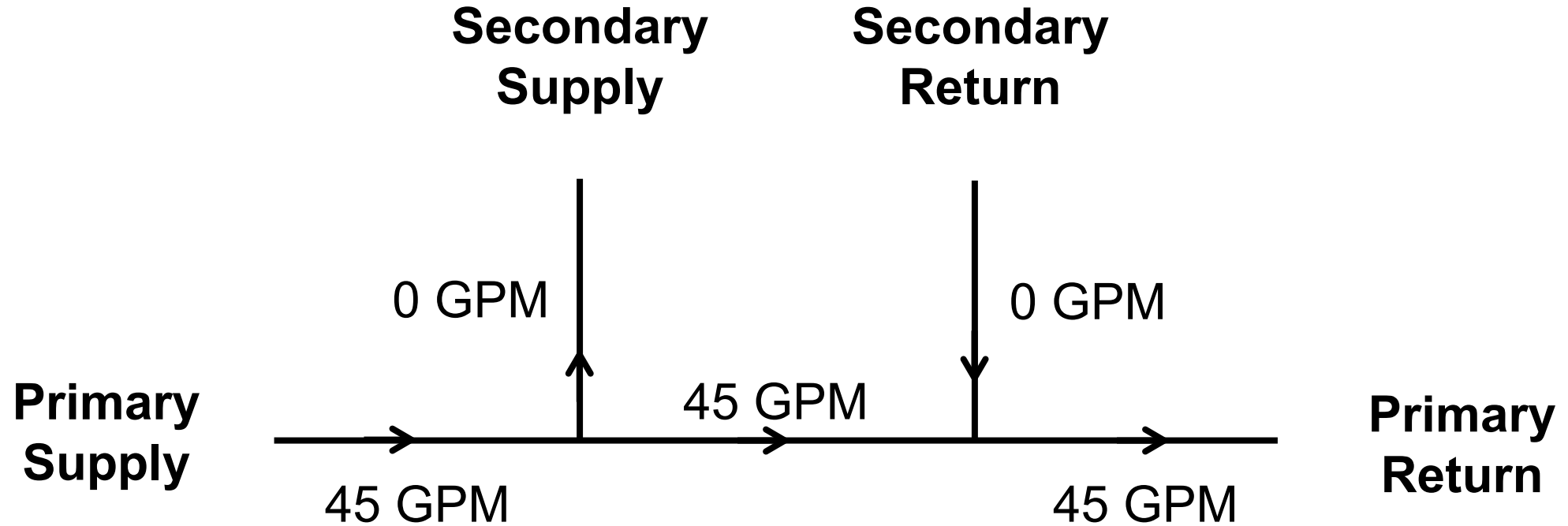
- “Reverse” Flow in the Common Pipe
- Secondary Supply Temp  $\neq$  Primary Supply Temp (**Mixing Tee**)
- Primary Return Temp = Secondary Return Temp (**Diverting Tee**)

# Secondary Flow

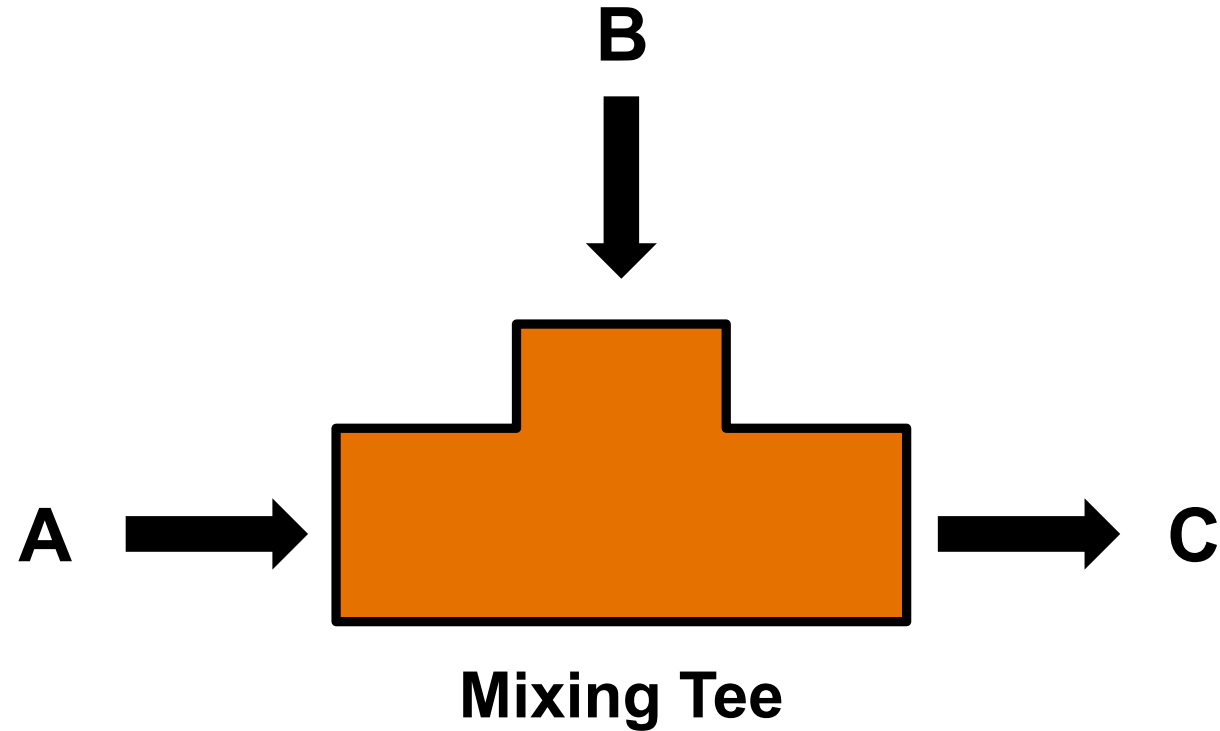


- “Forward” Flow in the Common Pipe
- Secondary Supply Temp = Primary Supply Temp (**Diverting Tee**)
- Primary Return Temp  $\neq$  Secondary Return Temp (**Mixing Tee**)

# \_\_\_ Secondary Flow



- “Forward” Flow in the Common Pipe
- No Secondary Flow
- Primary Return Temp = Primary Supply Temp



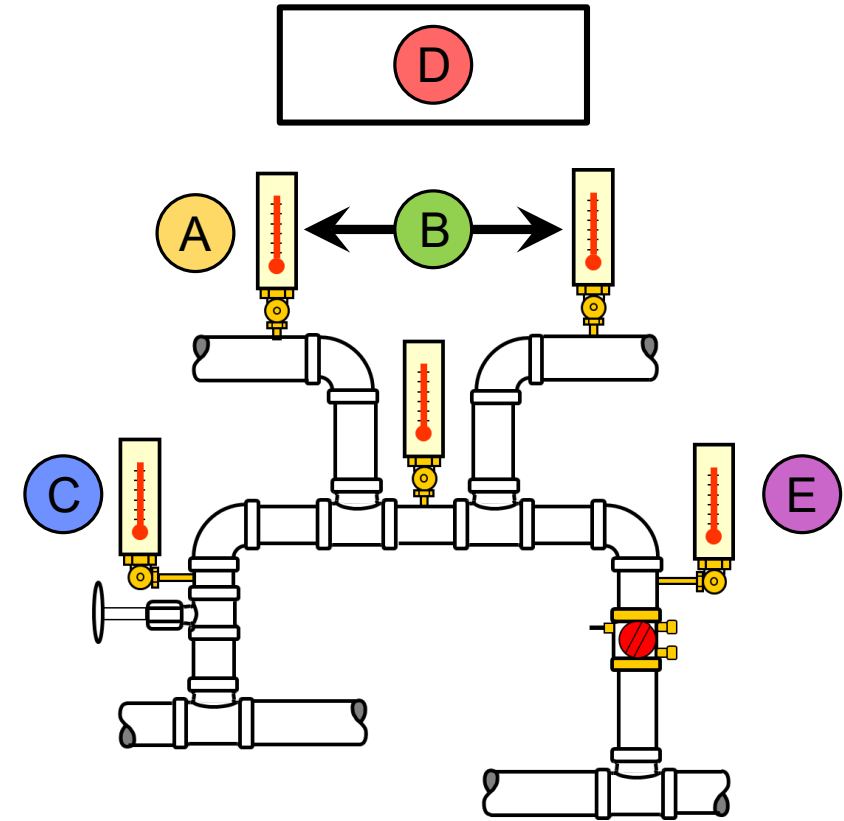
$$(\text{Flow}_C \times \text{Temp}_C) = (\text{Flow}_A \times \text{Temp}_A) + (\text{Flow}_B \times \text{Temp}_B)$$

$$\text{Temp}_C = \frac{(\text{Flow}_A \times \text{Temp}_A) + (\text{Flow}_B \times \text{Temp}_B)}{\text{Flow}_C}$$

- A. What is required supply water temperature to secondary load?
- B. What is the design  $\Delta T$  across secondary load?
- C. What is the primary supply water temperature?
- D. What is the total Btu/hr required for the secondary?
- E. What is the primary return temperature?

**Example:** A secondary load of 300,000 Btu/hr requires 55°F supply water and is designed for a 15°F  $\Delta T$ . The primary supply water from the chiller is 45°F.

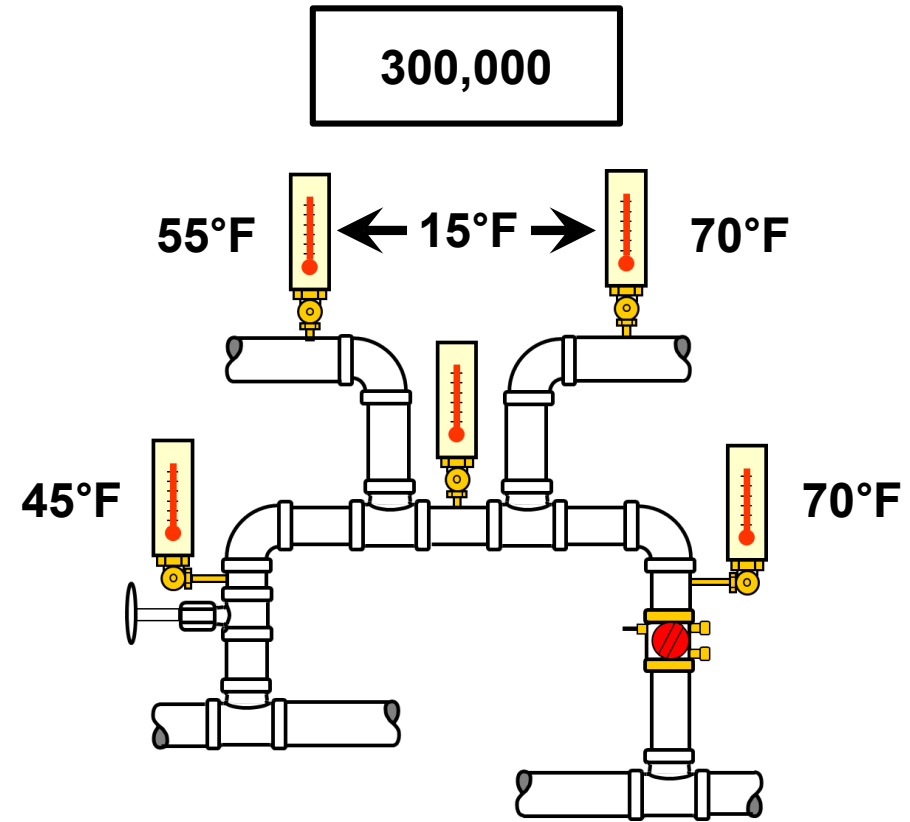
What is the required cross-over bridge flowrate?



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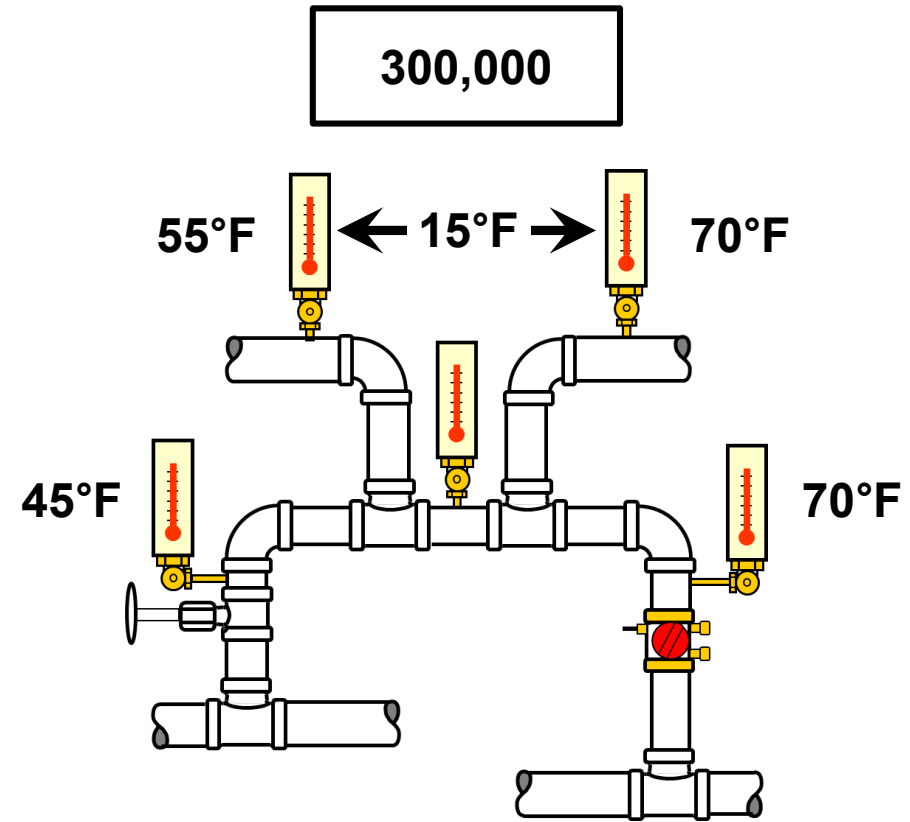


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**70°F - 45°F = 25°F  $\Delta T$  across the bridge**





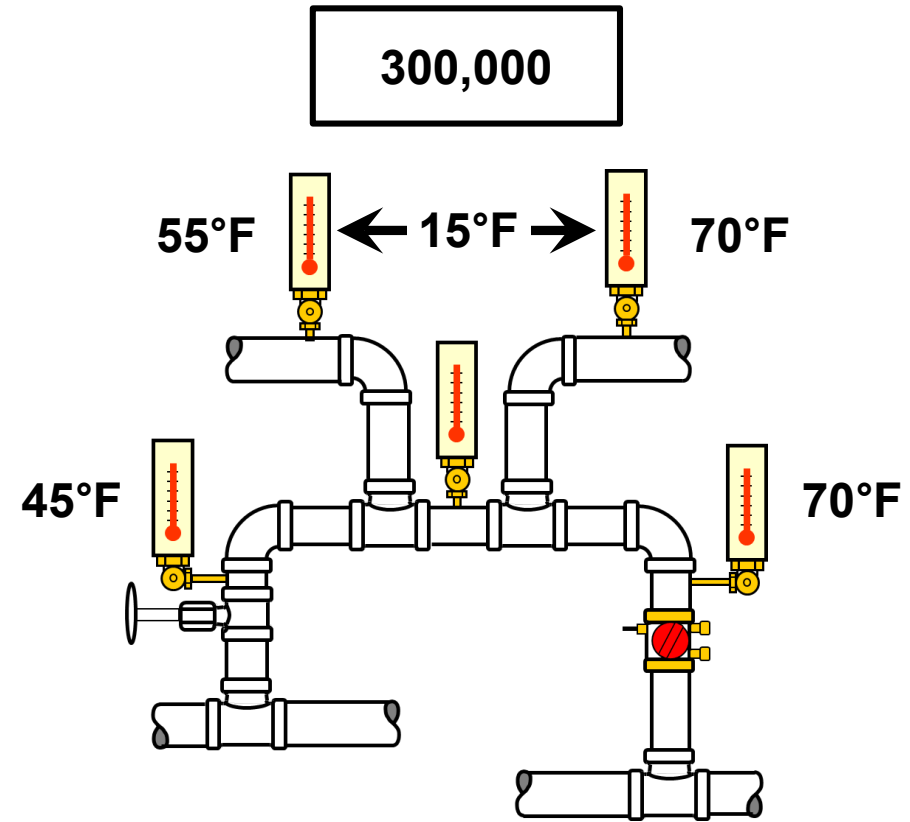
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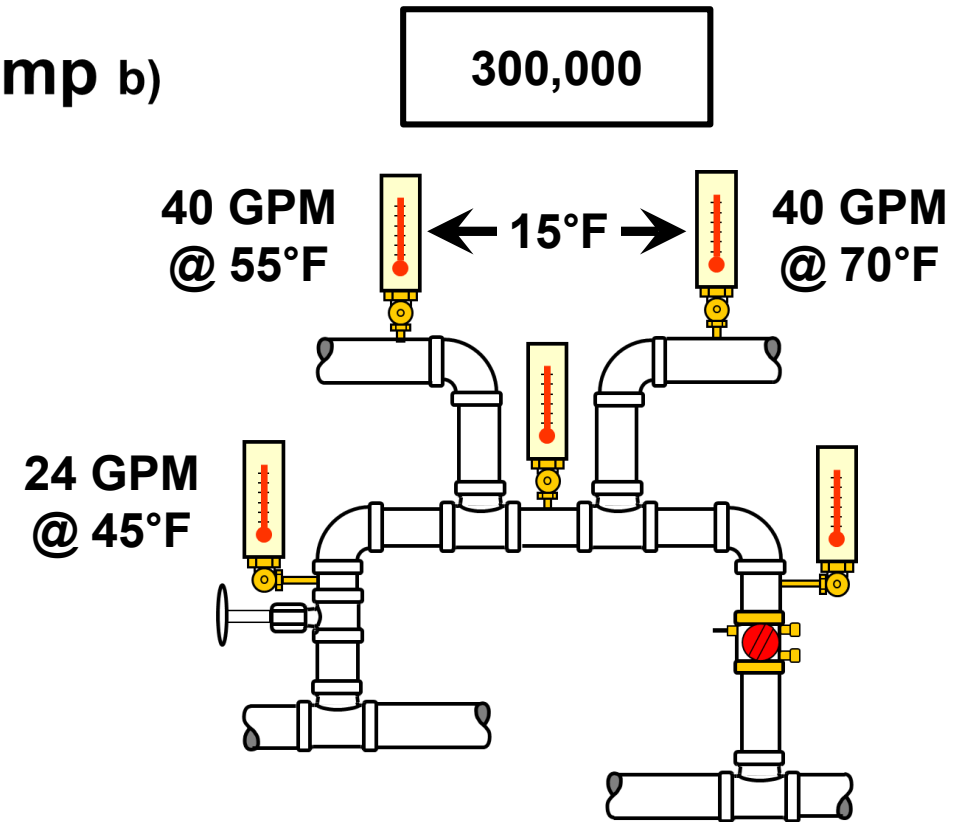
**70°F - 45°F = 25°F  $\Delta T$  across the bridge**

$$\frac{\text{Btu/Hr}}{500 \times \Delta T} = \text{GPM} \quad \frac{300,000}{500 \times 25} = \mathbf{24 \text{ GPM}} \text{ bridge supply from main}$$



$$\frac{300,000}{500 \times 15} = 40 \text{ GPM}$$

**Flow  $c$  x Temp  $c$  = (Flow  $a$  x Temp  $a$ ) + (Flow  $b$  x Temp  $b$ )**



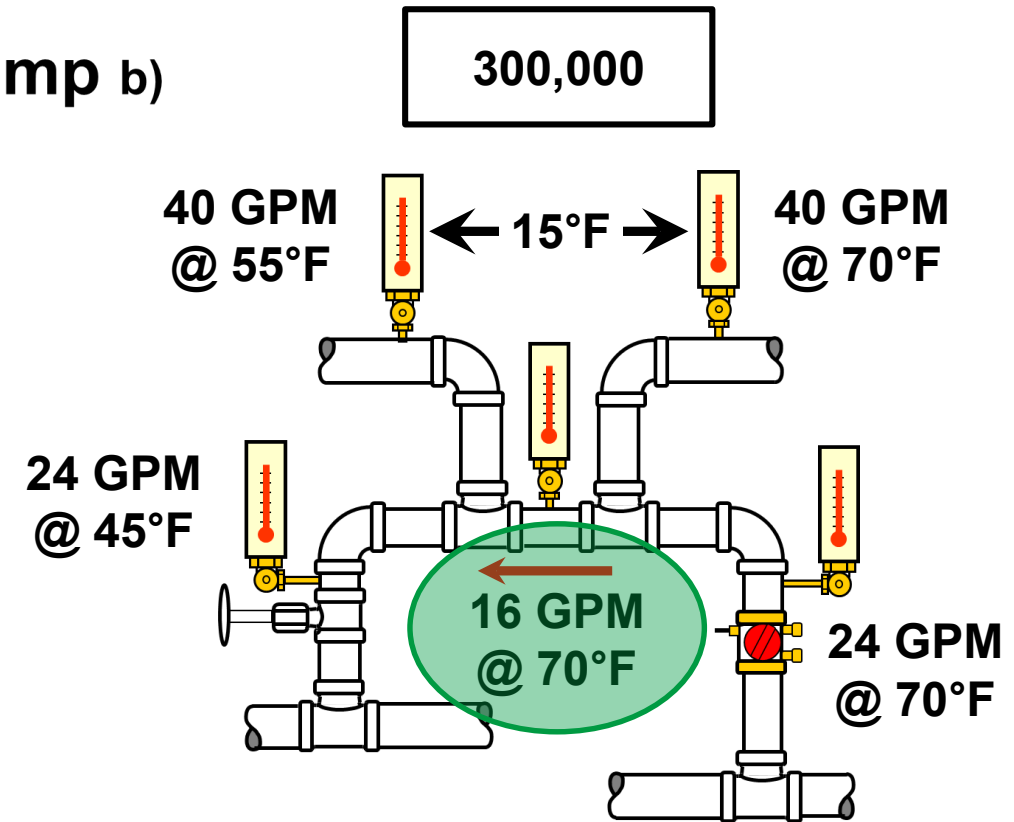
$$\frac{300,000}{500 \times 15} = 40 \text{ GPM}$$

$$\text{Flow}_c \times \text{Temp}_c = (\text{Flow}_a \times \text{Temp}_a) + (\text{Flow}_b \times \text{Temp}_b)$$

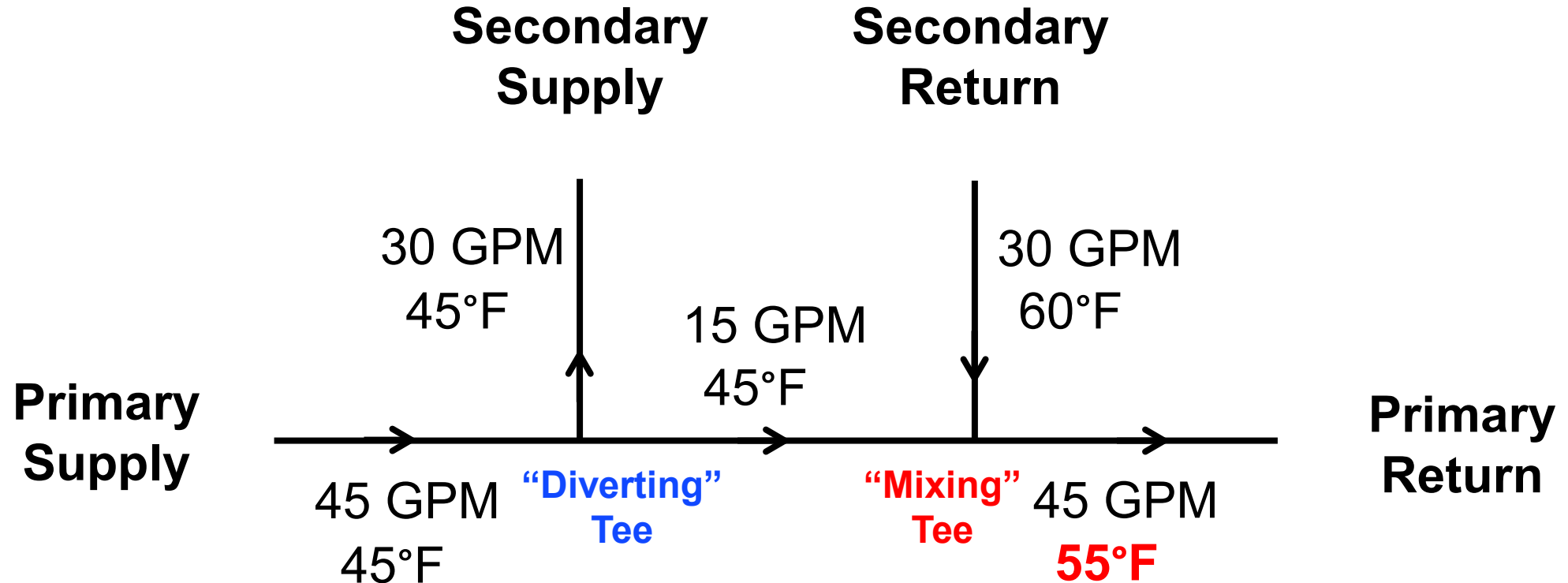
$$40 \times 55 = (24 \times 45) + (16 \times 70)$$

$$2200 = (1080) + (1120)$$

$$2200 = 2200$$



# Secondary Flow



- “Forward” Flow in the Common Pipe

$$\text{Temp}_c = \frac{(15 \times 45) + (30 \times 60)}{45} = 55.0^\circ\text{F}$$

- Secondary Supply Temp = Primary Supply Temp (Diverting Tee)

- Primary Return Temp  $\neq$  Secondary Return Temp (Mixing Tee)

## Typical Applications

- Large, diverse systems with high cumulative pressure drops
- Different Supply Water Temperatures in zones
- Stabilization of Boiler and Chiller flows required
- Freeze protection for Air Handling Coils

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## Benefits

- Design “large” primary loop temperature drops (*Smaller pump and piping*)
- Offers flexibility of Constant or Variable Speed Primary Pump operation
- Can reduce overall system pumping energy

